

Review

Recent Advances in Diagnostic Techniques and Condition Monitoring of Rotating Electrical Machines

ABSTRACT (ARIAL, BOLD, 11 FONT, LEFT ALIGNED, CAPS)

Electrical machines are critical components in industrial processes. A motor failure may yield an unexpected interruption at the industrial plant, with consequences in costs, product quality, and safety. To determine the conditions of each part of motor, various testing and monitoring methods have been developed. In this paper, a review on effective fault indicators and condition monitoring methods of rotating electrical machines has been accomplished. Fault detection methods divided to four groups: electrical, mechanical, chemical and thermal indicators. Some fault detection methods based on electrical symptoms like stator current, voltage, their combination or spectrum discussed in electrical group. In second branch, mechanical symptoms like torque, vibration and so on used for condition monitoring. Third group, chemical indicators, assigned to some chemical parameters of materials like oil characteristic or wear and debris in oil analysis. In last group, thermal symptoms in rotating electrical machines will be spoken. Between all methods, some of them are more known like vibration and some of them are recently added like motor current signature analysis (MCSA). Nowadays, combined methods and methods used artificial intelligence (AI) in condition monitoring are more popular. In every group, the fault detection method and the faults that can be detected have been mentioned. Mathematical equations of some new signal processing method have been discussed in literature presented in appendix.

Keywords: Condition monitoring, Electrical motor, Fault diagnosis, Review

1. INTRODUCTION

Fault diagnosis and condition monitoring have been studied in the recent decade to prevent costly interruptions due to motor faults and recognize faulty conditions as soon as possible 1–7.. Electrical motors are subjected to faults which may redound to secondary faults. The sources of motor faults may be internal, external or due to environmental conditions. Internal faults can be classified with reference to their origin.

Internal faults can be classified with their outbreak location: stator or rotor. Common machine faults in rotor according to 8. are:

- 1) Bearing failure;
- 2) Rotor broken bars;
- 3) Rotor body failure;

- 28 4) Bearing misalignment;
- 29 5) Rotor misalignment;
- 30 6) Bearing loss of lubrication;
- 31 7) Rotor mechanical or thermal unbalanced;
- 32 And common faults become apparent in stator as categorized in 8. are:

- 33 1) Frame vibration;
- 34 2) Stator earth faults;
- 35 3) Damage of insulation;
- 36 4) Stator turn-to-turn faults;
- 37 5) Stator phase- to- phase faults;
- 38 6) Displacement of conductors;
- 39 7) Failure of electrical connections;

40 These failures can be detected with several procedures. In this paper, they are discussed by
41 their detection method and parameters will be measured to four groups.

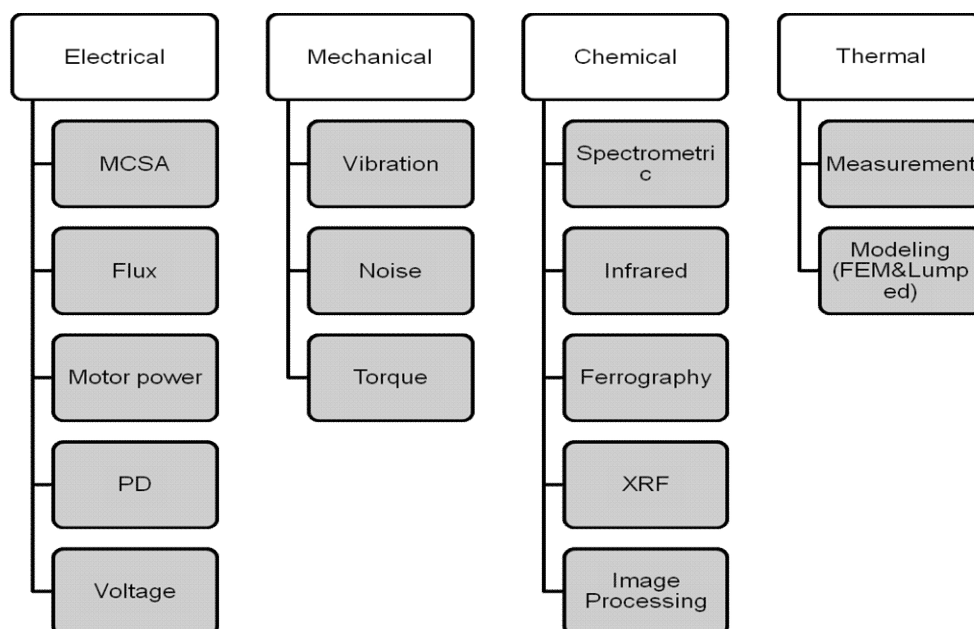
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43 2. FAULT DETECTION METHODS

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45 There are several indicators for faulty conditions of rotating electrical machines help us to
46 distinguish machine conditions. In this paper, fault detection methods persuaded by their
47 fault indicators. So condition monitoring method can be analyzed in four groups as
48 presented in Fig.1.

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52 2.1 Electrical analysis

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54 Some of the electrical faulty condition symptoms are motor current signature, voltage, flux,
55 power and so on. Probable faults can be detected by comparison between electrical signals
56 in healthy and unknown conditions.

57 Some of the electrical methods are based on signal injection and response analysis. For
58 instance, a method based on signal injection with high-frequency proposed in 9. for fault
59 detection in closed-loop drives, but it's difficult to implement for many applications due to
60 invasiveness and hardware limitations.

Akin et al. in 10. reported that the reference frame theory directly added into the main motor control subroutine in DSP program can successfully be applied to real-time fault diagnosis of electric machinery systems to find the magnitude and phase quantities of fault signatures even though in nonideal conditions such as offset, unbalance, etc.

In the rated rotor flux test by applying an ac voltage source across each side of the shaft, high shaft current and yoke flux have been utilized. This induces circulating current between the rotor bars and shaft, and the current or flux of each bar is indirectly monitored using iron filings/magnetic viewer or a thermal imaging camera. The influence of a cracked or broken bar or shorted rotor laminations can be observed by this test 11.. These methods are being done under standstill condition and don't seem efficient for online condition monitoring.

An automated technique for monitoring of rotor condition of voltage source inverter-fed induction machines at standstill has been proposed in 11.. In this algorithm, the motor is excited with a set of pulsating fields at a number of angular positions for observing the change in the impedance pattern for broken bar detection. This technique can be performed without any extra hardware but it's still an offline test.

2.1.1. Motor Current Signature Analysis (MCSA)

MCSA is one of the most popular approaches since it provides sensor less diagnosis of rotor problems 11.. MCSA requires the measurement and manipulation of lengthy steady-state data and an accurate measurement/estimate of the rotor speed for obtaining a reliable and high-resolution assessment but MCSA is not so effective for applications where the load constantly changes.

The prior MCSA techniques assume stationary and high SNR for signal. The nonstationary of stator current is accommodated by the commonly used windowing techniques 12.. The highly transient and dynamic nature of the induction motor stator current during fault conditions demand analysis through algorithms and techniques fit to analyze nonstationary and nonlocalized signals, such as wavelet transform or other time-frequency techniques. The availability of the advanced signal processing tools, such as higher order spectrum analysis 13., high-resolution or subspace methods 14. and wavelet analysis 15,16. have revolutionized the signal processing for fault detection in electrical motors.

MCSA usually has been attempted looking at $(1 - 2s)f$ and $(1 + 2s)f$ frequencies, lower sideband (LSB), and upper sideband (USB), which s is slip and f is main frequency 17..

The sideband amplitudes are affected by load level and power rating, constructive details, and by manufacturing asymmetries 18..

Because of the vicinity of signal main frequency to produced components and sidebands, broken bar detection may be difficult by this method 19.. Also, this problem exists under low slip operation. MCSA-based online rotor fault detection is not very effective since the current regulator masks the fault signatures in the current 20-22.. In addition, online monitoring techniques can fail if the operating frequency constantly changes due to adjustable speed operation. In 21,22., spectrum analysis of variable speed controller was proposed for rotor fault detection in field-oriented drives, but the methods can only be applied for a specific control scheme and are strongly influenced by controller parameters 23..

In 17. some new fault indicators for bar-breakage detection are exposed based on the sidebands of phase-current upper harmonics; the ratios $I_{(7-2s)f} / I_{sf}$ and $I_{(5+2s)f} / I_{7f}$ are examples

of such indicators, and they are independent on load torque and drive inertia. This method has low independence with respect to machine parameters and has linear dependence on fault gravity.

Jung et al. in 24. conducted an advanced online diagnosis system using MCSA and made up of the optimal slip-estimation algorithm, the proper sample selection algorithm, and the frequency auto search algorithm for more productivity.

In 25. have been compared different fault diagnosis methods like three phase current vector, the instantaneous torque, and the outer magnetic field. Finally, it's declared that MCSA can be the best method for diagnosis the rotor faults.

As a basic tool, various reference-frame-theory-based applications are reported in the recent studies, like finding deviation in an actual Concordia pattern used to determine the types and magnitude of faults in drive systems and stator, respectively 26,27., obtaining negative-sequence stator-fault-related indices from the line current 28., and detecting negative-frequency rotor asymmetry signatures at standstill based on complex fault signature vectors 29..

Time-frequency analysis has been investigated vastly in recent years but its complexity and heavy hardware requirements are limitations for simple low-cost drive systems 20..

There are several ways for data comparison in signal processing like Kolmogorov–Smirnov (KS) technique, Plateau algorithm, Holf–Winters (HW) technique and Mark–Burgess (MB) technique. If two time data series or distributions are at a significant variance the KS technique 30, 31., a nonparametric and distribution-free technique 32. is best choice. They are being used for comparison motor current signal with reference signal. The reference signal is motor current signal in healthy condition. The KS parameter is evaluated by taking the vertical difference between the two data distributions under test into consideration. The Plateau algorithm is apposite for handling long-term deviations and seems not suitable for condition monitoring. Holf–Winters (HW) algorithm is a forecasting technique needs a spontaneously event detection procedure, and Mark–Burgess (MB) technique is intended for detecting real-time changes. The KS technique is the best known of several distribution-free techniques that test general differences between data distributions. It is more valuable for applications, which are responsive to data distributions 12..

2.1.1.1. Order Tracking Method

Similar to vibration analysis in nonstationary condition or in variable speed motors instead of tracking absolute frequency, frequencies can be explained by multiple of a base frequency that is usually power source frequency. For instance this method in 33. used for detection inter-turn in Permanent Magnet Synchronous Motor (PMSM). In 33. by applying a Vold-Kalman Filter (VKF) 34. tried to use order tracking method for selected voltage and current harmonics and detect inter-turn in PMSM. Vold-Kalman Filter Order tracking (VKF-OT) beneficiary is that allows extracting both the amplitude and phase of the analyzed orders at each time instant directly from the original data. Furthermore, its tracking performance does not depend on the slew rate (rotational speed rate of change) 33. and make order tracking on noisy signal easy.

2.1.1.2. Time and Frequency Domain Analysis

There are some restrictions of the Fourier transform, for example it cannot be used for non periodic or nonstationary signals; otherwise, the resulting FFT spectrum will make little physical sense 15, 35, 36..

However, for machinery operating under unsteady conditions, because of variation in the rotating speed and operating load, even if the machine is in the normal state, the spectrum of the vibration signal is always altering in sampling time. When a nonstationary signal is transformed into the frequency domain, most of the information about the transient components of the signal will be lost 37., hence, a hybrid method has been proposed in 38..

Time-frequency analysis 39. methods can simultaneously generate both time and frequency information from a signal. Therefore, in later studies, time-frequency analysis methods are widely used to detect faults since they can determine not only the time of occurrence but also the frequency ranges of the location 40.. Time-frequency methods mostly use in

vibration analysis and MCSA. There are several time-frequency analysis methods, such as the Short-Time Fourier Transform (STFT), Wavelet Analysis (WA), and the Wigner-Ville Distribution (WVD), which may be used for condition monitoring of rotating machinery in transient and unsteady operating conditions. Those time-frequency techniques have been applied to fault diagnosis and condition monitoring in practical plant machinery 16,41,42.. Also Hilbert transform and Zhao–Atlas–Marks distribution in 43. applied to fault diagnosis of motors in nonstationary conditions but this method is not as common as prior methods. Misalignment detection using STFT and WA signal processing techniques is shown in Fig. 2 23..

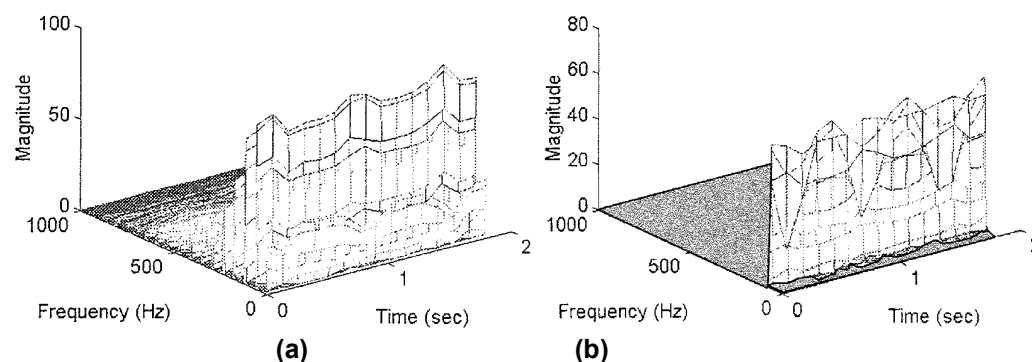


Fig.2. Misalignment detection using STFT and the wavelet technique:(a) STFT. (b) STFT and wavelet technique 3..

In the field of machinery fault monitoring, Wavelet Analysis (WA) has been used widely in the diagnosis of rolling bearings, gearbox and compressors. This technique also has been used for feature extraction and noise cancellation of the various signals 16,41-44..

In 16,41,45., a fault diagnostic technique for rotating machinery is investigated based on discrete wavelet transform. In Reference 46. a time-averaged WA according to Morlet continues wavelet used for fault diagnosis of a gear set. Also, reference 47. presents a combination of Continuous Wavelet Transform (CWT) and Kolmogorov-Smirnov test for fault detection of the bearings and gear box in transient conditions. In 44,48. CWT is used for extract the features of roller bearing fault signals. Reference 49. used CWT for fault signal diagnosis in an internal combustion engine.

In 50., the application of the Wigner-Ville distribution is reported to detect a broken tooth in a spur gear. Reference 51. shows that the WVD can be applied to the description of machine conditions and it is an effective method in machinery fault diagnosis. Reference 42. applies a PWVD to identifying the influence of the fluctuating load conditions for gearbox. A Digital Signal Processing (DSP) implementation is presented in 52. to detect mechanical load faults in induction motors during speed transients based on WVD and stator current analysis.

2.1.2. Flux Monitoring

Magnetic flux can be a fault indicator and monitored both inside the machine (search coils) or outside (axial coils). Coil installation and noisy spectra are the main difficulties 17.. One of the most applications of this algorithm is fault detection in rotor cage. The estimated rotor flux in 22. suggested for the diagnosis of rotor faults in vector-controlled drives. In 8. Dorell et al. showed a relation between air gap eccentricity and air gap flux and vibration signals. Cruz et al. in 53. presented an algorithm for diagnosis of rotor faults which starts with the measurement of the amplitude of the rotor flux oscillations. It's showed that the ratio between Δi_{ds} and the average value of Δi_{qs} , current changes in d and q axis respectively,

gives the degree of asymmetry of the motor or the number of adjacent broken bars, if the total number of rotor bars is known. But this algorithm needs some additional modules for calculating the current average values and tracks the amplitude of currents.

2.1.3. Motor Power Monitoring

Motor power signature analysis is focused on the detection of double-slip frequencies present in the electric input power spectrum 54. similar to MCSA. These harmonics are evaluated with respect to the average power (dc component), thus obtaining some fault severity factors. In addition, this method needs to acquire both currents and voltages. Also the dependence on the drive inertia is another limitation of this fault indicator 55.. Bellini et al. in 55. tried to detect rotor broken bar by this approach.

2.1.4. Partial Discharge (PD) Monitoring

This test mainly used in high voltage motors and generator stator windings. By using Partial Discharge Analyzer (PDA) sensors placed within the winding or at the winding terminals, stator winding PD pulses will separate from electrical interference (usually harmless) based on pulse arrival time or pulse shape and easily can be detected 56.. PD is a symptom of many stator winding insulation failure mechanisms. IEEE 1434-2000 reviews all types of PD measurement methods used in rotating machines 57..

There are several discharge monitoring techniques. Among these methods RF coupling method, capacitive coupling method and broad-band RF method 58. are more known. A Radio Frequency Current Transformer (RFCT) installed on neutral point of winding can detect Radio Interference Frequency Intensity (RIFI) caused by PD. Arcs occurred at any location cause RF current flow into the neutral point because of its low potential. The RIFI meter had a narrow bandwidth of about 10 kHz centered at 1MHz 58.. By using a frequency-based method with low power hardware, it is possible to take advantage of the RF technique without the need for wideband signal capture and its associated overheads 59..

Second method use specialized pulse height analyzer with bandwidth 80 MHz. In this approach connection to the winding is made through coupling capacitors at the machine line terminals 58.. Initially, the capacitors were connected to the machine during an outage, but latterly described how the capacitors could be permanently built into the phase rings of the machine and the measurements can be made without service interruption. In 60. showed that the pulse has a rise time (defined as 10%–90% of peak) of 4 ns and the frequency content of this pulse extends to over 100 MHz, thus, an 80-pF capacitor installed on high-voltage machine terminals can be used as the coupling device.

It has been shown that serious PD, sparking or arcing, has faster rise-times than the background corona and PD activity, and therefore produce a much higher bandwidth of electromagnetic energy, up to 350 MHz. If this energy is detected, at as high a frequency as possible, the ratio of damaging discharge signal to background noise is increased. Frequencies above 0.4 MHz do not propagate from the discharge place along the winding, as with the lower frequency techniques, but by radiation from the winding 58.. This radiation can be detected by an RF aerial located inside the enclosure of the machine or outside, close to an aperture in it and it is basic concepts of broad-band RF monitoring method.

2.1.5. Voltage spectrum analysis

The Growler test and rated rotor flux test with high current ac excitation are another commonly used offline tests for rotor testing 61-65.. A Growler is an electrical device used for testing insulation of a motor for shorted coils with an iron core and excited by AC current for detection insulation problem.

The method consists of inserting an auxiliary small winding which is a coil "sneak" that forms an angle θ_0 with the A stator phase as shown in Fig. 3 66.. This coil has no conductive contact with the other phases but it is mutually coupled with all the other circuits on both the stator and rotor sides 67..

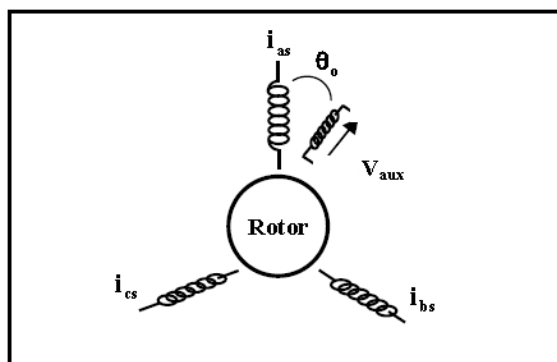


Fig.3. Auxiliary winding emplacement 67.

Mirimani et al. in 68. investigated the effect of static eccentricity on the back EMF of an Axial Flux Permanent magnet (AFPM) through 3D-FEM (Finite Element Method) as shown in Fig. 4 66.. The back EMF of the four coils of one phase is obtained to propose a suitable criterion for precise eccentricity fault detection.

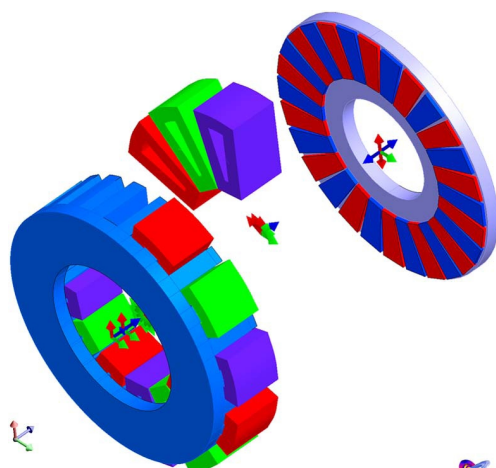
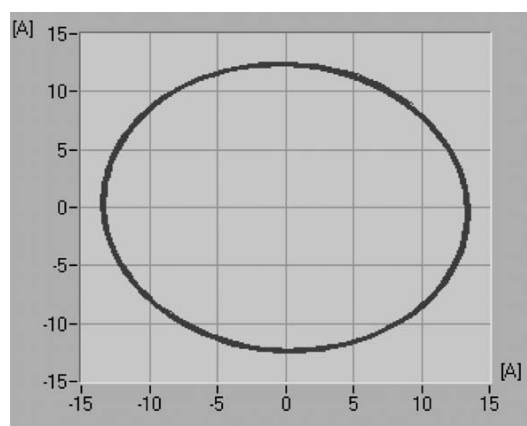


Fig. 4. 3D-FEM model of the axial flux permanent magnet motor 69.

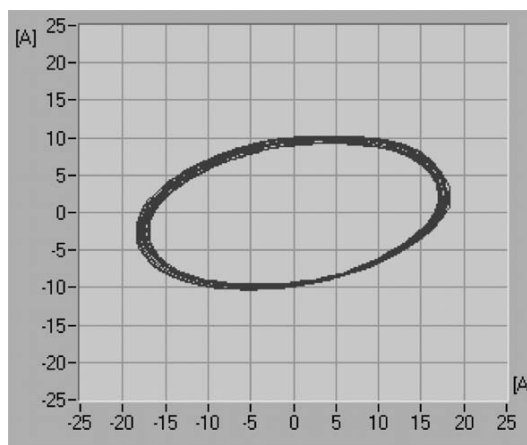
In the case of a healthy motor the auxiliary winding voltage Park components spectra contain one peak at the motor main supply frequency. The Lissajous curve is an ellipse as shown in Fig. 5 69.. In the different cases of voltage unbalances, the Lissajous curves are also ellipses that have different angles as shown in Fig. 6 69.. In comparison with damaged and non defected motor, the value of their superior and inferior radiuses will increase 66.. It is also well known that the effects of stator winding inter-turn faults may be detected by monitoring the Zero-Sequence Voltage Component (ZSVC) 70,71.. This method benefit is that it's separate from motor drive against some other methods like MCSA, but it needs to access to stator winding neutral point. In 33. attempted to detect inter-turn fault in PMSM by first harmonic amplitude of ZSVC and stator currents third harmonic. Briz et al. 72. used

284 voltage and current zero-sequence components for recognition of faults in induction
285 machine.
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288
289 **Fig. 5. Park's Currents Vector of a healthy motor 70.**
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293 **Fig.6. Park's Currents Vector for a motor with coils in shortcut 70.**
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297 **2.2. Mechanical Analysis**

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299 There are several mechanical symptoms for faulty condition of electrical machine, such as:
300 vibration, noise, torque and so on.
301

302 **2.2.1. Vibration Monitoring**

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304 As almost 80 percent of common rotating equipments problems are related to misalignment
305 and unbalance, vibration analysis is an important tool that can be used to eliminate recurring
306 problems 73,74.. In many cases, the overall vibration level of the machine is sufficient to
307 diagnose mechanical failures 75,76., but in 2. showed that this is not an efficient method for
308 all faults. In 77. showed that the electromagnetic force is the most sensitive indicator of air
309 gap eccentricity. Therefore identifiable signatures should be found in the vibration pattern of
310 rotating electrical machines. The only drawback of this indicator is its low accessibility.

311 Nevertheless, since vibrations are the consequences of the forces on the machine structure,
 312 identifiable signatures should be found in the vibration pattern. The measured vibration and
 313 associated current harmonics are closely correlated 12..
 314 Literature survey 78-81. shows that most of the bearing fault diagnoses are based on
 315 vibration analyses like wavelet transform and Hilbert–Huang transforms or current-based
 316 analysis.
 317 In 82. illustrated how eccentricity faults can be identified from vibration analysis using
 318 condition monitoring techniques.
 319 The overall RMS of vibration can be calculated by different definition based on the spectrum
 320 in frequency domain across all of the effective frequency range, i.e., from DC to maximum
 321 analysis frequency range. One of the suggested formulas is 83.:

$$322 \quad overallRMS = \sqrt{\frac{\sum_{0}^{0.45 \times f_s} power(f)}{BW}} \quad (1)$$

323 In above equation, BW is noise power bandwidth of window, f is analysis frequency band
 324 and f_s is sampling frequency band.

325 Another special frequency analysis is Cepstrum that defined:

$$326 \quad C(\tau) = \left| F^{-1} \{ \log(|F\{f(t)\}|^2) \} \right|^2 \quad (2)$$

327 This can be used for examining behavior of gearboxes 19..
 328

329 **2.2.1.1. Frequency-Domain Analysis**

330
 331 The most common tools of vibration monitoring in industrial plants is frequency analysis.
 332 Finley et al. 84. compiled a resume table with a comprehensive list of electrically and
 333 mechanically induced components in the vibration pattern. Their analysis is based on
 334 analytical formulas.

335 In 85., a strategy presented based on monitoring slot passing frequencies in high frequency
 336 vibration components. Their presented analysis was based on rotating wave approach
 337 whereby the magnetic flux waves in the air gap are taken as the product of permeance and
 338 Magneto Motive Force (MMF).

339 Vibration pattern for the healthy motor and with dynamic eccentricity has been compared in
 340 86. as shown in Fig. 7. In paper 86. has been showed that the low frequency components of
 341 vibration (measured by accelerometers fixed on the outer casing of motor) can be used as
 342 signatures for the detection of eccentricity in induction motors.

344 **2.2.1.2. Order Tracking Methods**

345
 346 The advantages of order tracking over the other vibration techniques mainly lie in analyzing
 347 non stationery noise and vibrations which will vary in frequency and amplitude with the
 348 rotation of a reference shaft. The analysis of non stationery conditions needs additional
 349 information, as compared to steady state conditions, for an accurate result to be obtained.
 350 Order domain analysis relates the vibration signal to the rotating speed of the shaft, instead
 351 of an absolute frequency base 19..
 352

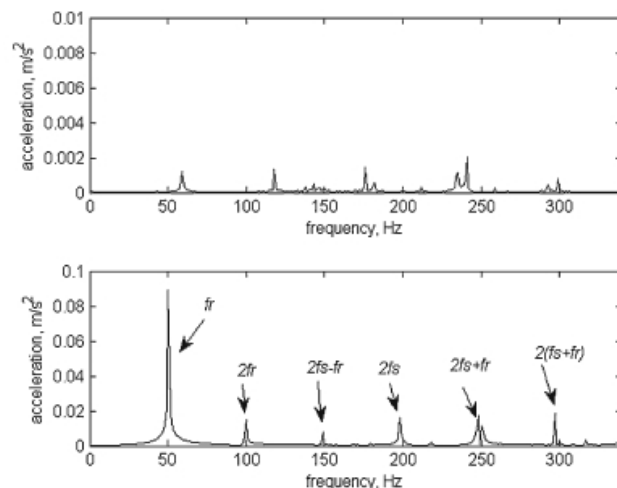


Fig.7. Vibration pattern for healthy motor (top) and with 37% dynamic eccentricity (bottom), 1.9% and motor fed at 100Hz in both cases 87.

2.2.2. Noise Monitoring

Measuring and analyzing the acoustic noise spectrum is another method of condition monitoring in rotating electrical machinery which require special consideration. Acoustic noise emitted from air gap can be an indicator of probably eccentricity in induction motor. But, the application of noise measurement in a noisy environment like a plant is not so efficient. In 87. an approach for air gap eccentricity detection presented and a test carried out in an anechoic chamber. Slot harmonics in the acoustic noise spectra were introduced as an indicator of static eccentricity. Li and He 1. used Hilbert-Huang Transform (HHT) for analyzing nonstationary noise signals incorporates a threshold-based denoising technique to increase the SNR for health monitoring in electrical machines.

Reference 88. examines whether acoustic signal can be used effectively to detect the various local faults in gearboxes using the smoothed Pseudo Winger-Ville Distribution (PWVD).

Scanlon et al. 89. showed that by extraction hide information of acoustic noise signal can predict machinery resident life time.

Defects in the roller element bearings cause particular frequencies to be excited. These frequencies can be detected in acoustic noise spectrum. In 90., an automated approach to degradation analysis is proposed that uses the acoustic noise signal from a rotating machine to determine the remaining useful life of the machines.

2.2.3. Torque Monitoring

By comparison between the estimated torque from the model and measured torque can detect some faults in electrical motors, so it's necessary to have a good model and an algorithm to be aware of air gap real torque. The electromagnetic torque estimation has been commonly used in electrical drives to control the torque and the rotor speed of AC electrical machines. So, it is needed to compute stator flux or rotor flux exactly in which the accuracy and the robustness are directly related to electrical machine parameters 91.. In addition, the flux estimation needs to have knowledge about only two parameters of these three parameters: stator phase voltages, currents, and the rotor speed by using an appropriate model 92..

In reference 93. torque estimation beside torsional vibration analysis used for gearbox fault detection in traction system and by measuring the torque their work has been validated.

391 Guzinski et al. in 94. for identification problems related to transmission system in High Speed
392 Train (HST) used the load torque observer without adding any additional sensors. The
393 presented observer system was able to detect the meshing frequency of the test bench
394 which has very small amplitude in the tested healthy gear.

395 From the input terminals, the instantaneous power includes the charging and discharging
396 energy in the windings. Therefore, the instantaneous power cannot represent the
397 instantaneous torque. From the output terminals, the rotor, shaft and the mechanical load of
398 a rotating machine constitute a torsional spring system. This torsional spring system has its
399 own natural frequency 95.. The attenuation of the components of the air gap torque
400 transmitted through the torsional spring system is different for different harmonic orders of
401 torque components 96,97..

402 The locked-rotor torque and breakdown torque will decrease in unbalanced voltage situation.
403 If the unbalanced voltage was extremely severe, the torque might not be adequate for the
404 application although the full-load speed is reduced slightly when the motor operates with
405 unbalanced voltages 98. and it can be an indicator of unbalance voltage condition.

406

407 **2.3. Chemical Indicators**

408

409 Insulation degradation can be monitored chemically by the presence of special matter in the
410 coolant gas or by detection some particular gases such as ozone, carbon monoxide or even
411 more complex hydrocarbons, like acetylene and ethylene 58.. Electrical discharge activity,
412 heat and some other electrical and mechanical faults may lead to insulation degradation.
413 The product materials can be gas, liquid or solid. Each of them needs a particular detection
414 method.

415 An ion chamber was designed in 99. to detect the products of heated insulation and it was
416 applied to a large turbo generator.

417 The metal wear debris in oil can be classified ferromagnetic wear debris and
418 unferromagnetic wear debris. When wear debris is in the coil of inductive wear debris
419 sensor, the magnetic field distribution of the coil is changed, and then the equivalent
420 inductance of the coil was changed. This technique for metal wear debris in oil is a
421 noncontacting and quick method and can be off-line and on-line 100..

422 In addition oil particle can be detected for fault diagnosis. With modern diagnostic tools, oil
423 analysis is used to monitor the condition of equipment as well as condition of a lubricant.
424 Various faults such as misalignment, unbalance, overload or accelerated heating condition
425 may lead to wearing in electrical machinery. The different types of wear are: abrasive wear,
426 adhesive wear, cavitations, corrosive wear, cutting wear, fatigue wear and sliding wear 73..
427 Some types of oil analyses are: viscosity, solids content, water content, total acid number,
428 total base number and flash point 73..

429 As mentioned, wear particles are the prime indicators of the machine's health. There are
430 many techniques to evaluate the type and concentration of such particles. The techniques
431 include: spectrometric analysis, infrared analysis, X-ray fluorescence (XRF) spectroscopy,
432 particle counting, direct reading ferrography and analytical ferrography 73..

433

434 **2.3.1. Spectrometric analysis**

435

436 This is one of the main techniques that typically reported in PPM (Parts Per Million). This
437 technique generally monitors the smaller particles and large wear metal particles present in
438 the oil will not be detected.

439 For larger wear particles, there are available techniques such as: acid digestion method,
440 microwave digestion method, direct read (DR) ferrography and Rotrode filter spectroscopy
441 (RFS).

442

443 **2.3.2. Infrared analysis**

444
445 Specific groups of atoms called functional groups by this method can be detected. An
446 appropriate wavelength is directed at the sample being analyzed, and the amount of energy
447 absorbed by the sample is measured. The amount of absorbed energy is an indication of the
448 extent of presence for that particular functional group in the sample. It is hence possible to
449 quantify the results. This analysis was first introduced in 1979. After several years a new
450 method extracted from this analysis named Fourier Transform-Infrared Analysis (FT-IR). By
451 this technique, a beam of light is focused through a film of used oil and the wavelengths are
452 then compared to light transmitted through new oil of the same type. The differences in
453 readings provide information with respect to the degradation of the used oil 73..
454
455

456 **2.3.3. Wear Particle Analysis (WPA) or Ferrography**

457
458 Ferrography or WPA utilizes microscopic analysis to evaluate the particles type, shape, size
459 and quantity. The components specifications allow a process of elimination in which the
460 abnormal wear can be identified. This analysis is used in two ways: A routine monitoring and
461 trending of the solid contents, Observing and analyzing the type of wears 73,101..
462

463 **2.3.4. XRF (X-ray fluorescence) spectroscopy**

464
465 The XRF spectroscopy entails the excitation of electrons from their orbits. This leads to
466 emission of UV rays with characteristic frequencies, which can be analyzed. During Rotrode
467 atomic emission spectroscopy, an electrical discharge produces plasma, causing thermal
468 emission. When the atoms return to the normal state, the excess energy is emitted as light.
469 Each element emits light at different frequencies on the electromagnetic spectrum. The
470 amount of light emitted at a given frequency corresponds to the concentration of the element
471 present in the sample. Also atoms can be excited by bombardment of X-rays 73..
472

473 **2.3.5. Image Processing**

474 The image processing and computer vision system reveals more information in the form of
475 quantitative data not revealed by the human eye. This technique is used to collect
476 quantitative information from wear particle images. Image analysis system is developed to
477 process and store the information of particle shape and edge detail features. In 102.
478 particles have been defined as regular, irregular, circular and elongated. So, an image
479 processing technique is applied for analyzing wear debris.
480

481 **2.4. Thermal Monitoring**

482
483 Due to thermal limitation of various parts of rotating electrical machines such as insulations,
484 coil and so on, it's necessary to have a good idea about machine parts temperature.
485 Thermal monitoring for electrical machines has two aspects, measuring the temperature and
486 thermal modeling, which each one of them has been illustrated shortly.
487

488 **2.4.1. Temperature Measurement**

489
490 There are three main approaches for temperature measurement in electrical machines: 1)
491 Measuring local point temperatures by embedded temperature detectors (ETD) or resistance
492 temperature detectors (RTD); 2) Using thermal images, fed with suitable variables, to
493 monitor the temperature of the perceived hottest spot in the machine; 3) Measuring
494 distributed temperatures of the machine or bulk temperatures of the coolant fluid 58..

These demonstrate the fundamental difficulty of temperature monitoring; the conflict between easily made point measurements, which give only local information, and bulk measurements that are more difficult and run the risk of overlooking local hot-spots. Choosing location of settling detectors requires careful consideration during specification. Bulk measurement can be found from the measurement of the internal and external coolant temperature rises, obtained from thermocouples located. Milic and Srechovic in 103. presented a new non-contact measurement system for hotspot and bearing fault detection in railway traction system (RTS). Of course, due to rotating parts in electrical motors, these methods are not efficient and thermal modeling is inevitable.

2.4.2. Thermal Modeling

Generally, thermal models of electric machines are classified into two categories 95,104.:

- 1) Finite Element Analysis (FEA) based model
- 2) Lumped Parameter (LP) thermal model

Finite Element Method (FEM) or Finite Difference Method (FDM) tools have traditionally been used to model the thermal performance of electric machines. Their applications have been limited only to small sectors of the stator and rotor and have not shown full-scale simulation for motors with complicated geometry. The accuracy of model is generally dependent on the number of thermally homogenous bodies used in model 105, 106.. By this work, researcher may simplify the complicated geometry and shorten computational time for constructing elements and calculating large system matrices.

On the other hand lumped parameter equivalent thermal circuit is easy to solve and gives a good overall view of the temperature rise in different parts of the machine without much computational time 107.. Chowdhury claimed that the lumped parameter thermal equivalent circuit proposed in 108. is easy to visualize as all the parameters are directly derived from the machine geometry. Boglietti et al. 104. compared the LP and FEA for thermal modeling of electrical machines.

There are two ways for extraction parameters of lumped parameter model. The first one is by using comprehensive knowledge of the motors, physical dimensions and construction materials. The second one is to identify the parameters from extensive temperature measurement at different locations in the motor explained in previous session. Even though an electric machine is made up of various materials that have different characteristics, the machine can be assumed to consist of several thermally homogenous lumped bodies 95.. For example, a simplified model of an induction model and a PMSM consisting of two lumped thermal bodies are presented in 109,110.. Likewise in 111., Milanfar and Lang developed a thermal model of electric machine to estimate the temperature of the motor and to identify faults like turn-to-turn faults and bearing faults.

A time-domain lumped thermal model of an induction motor obtained in 112.. The temperature distribution and the energy destruction are shown in Fig. 8.

Nategh et al. in 113. presented a lumped parameter thermal model for a permanent-magnet assisted synchronous reluctance machine (PMSRM) developed for propulsion in a hybrid electric vehicle. They divided the stator slot into a number of elliptical copper and impregnation layers and modeled stator winding by some approximation.

Jankowski et al. 112. described the development of a time-dependent lumped-parameter thermal model of an induction motor, and showed that how this thermal model can be used to minimize the internal temperature during operation.

Kolondzovski et al. in 114. discussed about thermal issues of different types of electric motors and different rotor types. Similarly, EL-Refaie et al. in 115. presented multibarrier interior permanent magnet machines lumped parameter model.

Idoughy et al. 116. proved that the analytical techniques may risk underestimating the hotspot winding temperature, especially when the fill factor is below 0.3. In addition, the

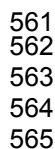


Fig.8. Thermal model of an induction motor in the flow loop 3 h after startup. The temperature distribution is shown in (a), and the energy destruction is shown in (b)

3. MODEL BASED & AI-BASED METHODS

A model-based fault monitoring method presented in 122. for variable speed drives without frequency analysis. Nowadays, AI-based which use fuzzy logic, neural network, particle swarm optimization 123. and so on are so popular for researchers. Some of them are explained in this paper.

3.1. Artificial Neural Network

Nejjari et al. in 124. used learning Park's vector pattern based on artificial neural network to discern healthy and faulty patterns. Also, Wang et al. in 125. used combination of these two algorithms for condition monitoring of rolling bearings.

Tag Eldin et al. 126. used Artificial Neural Network and applied result of the RMS measurement of stator voltages, currents and motor speed to train a neural network to monitor and diagnosis external motor faults.

Asiri 127. decided to detect six different types of PD using neural networks and classify different types of PD according to the location of PD activity.

3.2. Fuzzy logic

The fuzzy logic tool provides a technique to deal with imprecision and recently attracted researchers attention for different applications like fault diagnosis. The utility of fuzzy sets lies in their ability to model uncertain and vague data. Fuzziness in a fuzzy set is characterized by its membership functions as shown in Fig. 9 128..

An extraction method based on the Relative Crossing Information (RCI) in 129. proposed for condition monitoring of a machine under the variable rotating speed, by which the instantaneous feature spectrum can be automatically extracted from the time-frequency distribution of the fault signal. The performance of this approach is evaluated using three time-frequency techniques, namely STFT, WA, PWVD and finally using a sequential fuzzy diagnosis method.

Reference 130. claimed that using fuzzy sets and uncertainty phenomena with possibility theory may help in fault diagnosis of satellite applications. A combination of neural network and fuzzy logic used in 125. for condition monitoring of rolling bearings. Also, 131. propounds an intelligent condition diagnosis method for rotating machinery developed using least squares mapping (LSM) and a fuzzy neural network. In 129., possibility theory is also applied to combine with PWVD technique for fault diagnosis.

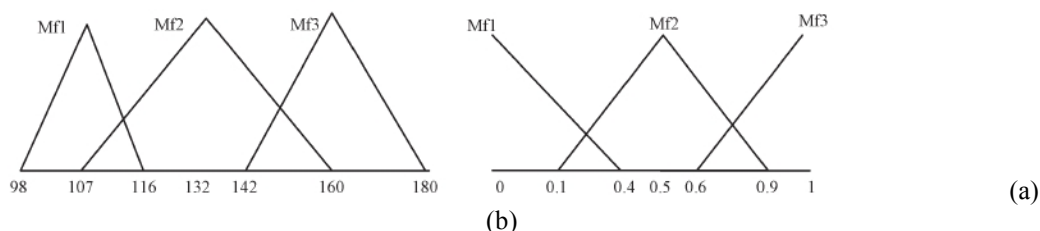


Fig.9. Membership functions of (a) input nodes and (b) output nodes of the fuzzy inference system 127..

4. CONCLUSIONS

Condition monitoring methods for rotating electrical machines have been surveyed in four groups. These groups consisted of: electrical analysis, mechanical analysis, chemical analysis and thermal analysis. In each group, there are several symptoms that faulty condition in machines can be detected by them.

Methods based on signal injection seem profit for fault detection in closed-loop drives, but it's difficult to implement for many applications due to invasiveness and hardware limitations.

MCSA, the most popular technique, provides sensor less diagnosis of some motor problems but it's not so effective for applications where the load constantly changes. Time-frequency analysis has been investigated vastly in recent years but its complexity and heavy hardware requirements are limitations for simple low-cost drive systems.

Motor power analysis because of need to both currents and voltages simultaneously and dependence on the drive inertia has some limitation. PD monitoring mainly used in high voltage motors and generator stator windings. Most of recurring problems in rotating machinery like misalignments can be detected by vibration analysis. The measured vibration and associated current harmonics are closely correlated. By detection ozone, carbon monoxide and others in the coolant gas or oil analysis, some faults like insulation degradation can be detected easily. Also thermal measurement and thermal modeling are introduced as efficient tools for motors condition monitoring. Finally, AI- based algorithms combined of one or more explained methods were studied.

Besides these methods and algorithms, nowadays web-based monitoring approaches are interesting. They are using one or more of these mentioned procedures in softwares like LabVIEW, as you see in 132. and shown in Fig. 10.

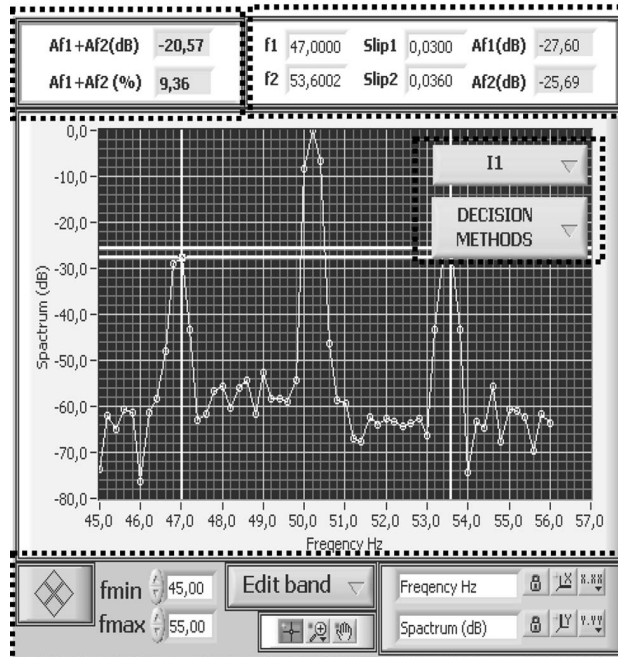


Fig.10. Diagnosis session panel with decision method menu presented in 131.

644 Appendix

645

646 Time-Frequency Analysis method equations which discussed at this paper are explained in
647 this session.

648

649

650 1) Short-Time Fourier Transform (STFT):

651 The short-time Fourier transform (STFT) 39. by breaking signal into short blocks and
652 applying an FFT to each part can determine the sinusoidal frequency and phase component
653 of the its local time domain.

654 Mathematically, the STFT of a signal $x(t)$ is explained as follows 40.:

$$655 \quad STFT_x(t, \omega) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{+\infty} x(t)h(\tau - t) \exp(-j\omega\tau) d\tau \quad (3)$$

656 In the above equation ω is an angular frequency, and $h(\tau)$ is the window function. With the
657 technique of windowing (such as Gaussian, Hamming, Hanning ...), the STFT can provide
658 information about both time and frequency of the signal, since the time-varying concentration
659 information is required for real-time applications. STFT analysis may lose the transient and
660 temporal information and it is not good, but the STFT is simpler than the other methods. The
661 STFT spectrum can be defined as follows 40.:

$$662 \quad P_x(t, \omega) = |STFT_x(t, \omega)|^2 = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{+\infty} x(\tau)h(\tau - t) \exp(-j\omega\tau) d\tau \quad (4)$$

663 Of course other studies 133,134. showed that the techniques such as short-time Fourier
664 transform, where a nonstationary signal is divided into short pseudo-stationary segments,
665 are not suitable for the analysis of signals with complex time–frequency characteristics.

666

667 2) Wavelet Analysis (WA)

668 WA is another time-frequency signal analysis method that has been widely used and
669 developed recent decade. It has the local characteristic of the time domain as well as the
670 frequency domain, and its time-frequency window is changeable. The Continuous Wavelet
671 Transform (CWT) of $x(t)$ is a timescale method of signal processing that can be defined
672 mathematically as the sum over all time of the signal multiplied by scaled and shifted
673 versions of the wavelet function $\psi(t)$ 40.:

$$674 \quad CWT_x(a, b) = \frac{1}{\sqrt{|a|}} \int_{-\infty}^{+\infty} x(t)\psi^*\left(\frac{t-b}{a}\right)dt \quad a, b \in R \quad (5)$$

675 Where $\psi^*(t)$ is the complex conjugate of which denotes the mother wavelet or basic
676 wavelet. a & b are parameters related to scale and time respectively. If a is small, higher-
677 frequency components can be analyzed, and when it is large, lower-frequency components
678 can be analyzed. When b is given a value, the fundamental function can be shifted by a
679 distance in the direction in which time advances. The CWT spectrum is considered as
680 follows. Wavelet transform has the isometric characteristic.

681

682 3) Winger-Ville Distribution (WVD):

683 The Wigner-Ville Distribution (WVD) 39. is a very important quadratic-form time-frequency
684 distribution with optimized resolution in both the time and frequency domains. The WVD is
685 matched to linear chirps and can represent it effectively. The instantaneous frequency of
686 such signals can be estimated easily by picking the peak in the time-frequency plane 40..

687 However, the WVD does not yield a localized distribution for frequency variations that are
688 not linear 42,129..

689 The instantaneous frequency within the window can be considered to be nearly linear
690 because the VWD variants need windowing.

691 The Pseudo-Wigner-Ville distribution (PWVD) has better resolution and provides a more
692 accurate estimate of the instantaneous frequency. Therefore, it has been used extensively in
693 various applications to display time-frequency spectral information 15.. The PWVD equation
694 defined as follows 95,135.:

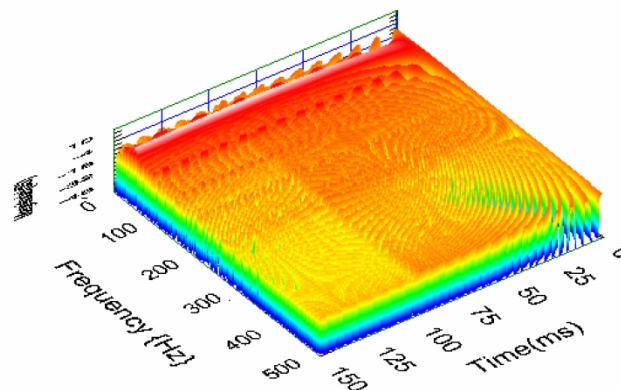
$$695 \quad PWVD_x(t, \omega) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} x^*(t - \frac{1}{2}\tau) x(t + \frac{1}{2}\tau) h(\tau) e^{-j\omega\tau} d\tau \quad (6)$$

696 In this equation ω is an angular frequency and $h(\tau)$ is the windows function.

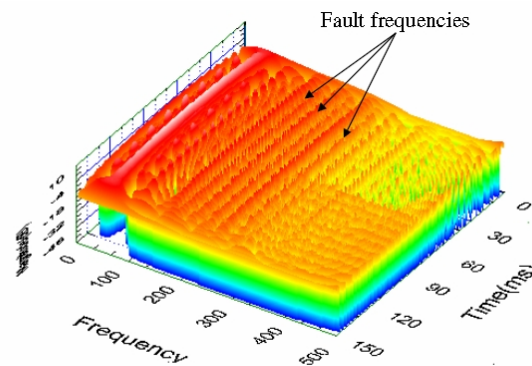
$$697 \quad W(t, \omega) = \frac{1}{2\pi} \int s^*(t - \frac{1}{2}\tau) s(t + \frac{1}{2}\tau) e^{-j\omega\tau} d\tau = \frac{1}{2\pi} \int S^*(\omega - \frac{1}{2}\theta) s(\omega + \frac{1}{2}\theta) e^{-js\theta} d\theta \quad (7)$$

698 Winger-Ville distribution of a motor in healthy condition and with faulty bearing is shown at
699 Fig. 11 95..

700
701



(a)



(b)

Fig.11. Winger-Ville distribution of motor (a) in healthy condition (b) Winger-Ville distribution of motor with faulty bearing 95.

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REFERENCES

1. Li, Ruoyu, and David He. Rotational Machine Health Monitoring and Fault Detection Using EMD-Based Acoustic Emission Feature Quantification. *Instrumentation and Measurement, IEEE Transactions on* 61.4 (2012): 990-1001.
- 2.S.A. Mortazavizadeh, A. Vahedi and A. Zohouri, Detection of Stator Winding Inter-turn Short Circuit In Induction Motor Using Vibration Specified Harmonic Amplitude , 2nd International Conf. on Acoustics & Vibration, Sharif Univ. of Technology, Tehran, Iran, Dec. 2012.
3. El Hachemi Benbouzid, Mohamed. A review of induction motors signature analysis as a medium for faults detection. *Industrial Electronics, IEEE Transactions on* 47.5 (2000): 984-993.
4. Nandi, Subhasis, Raj Mohan Bharadwaj, and Hamid A. Toliyat. Performance analysis of a three-phase induction motor under mixed eccentricity condition. *Energy Conversion, IEEE Transactions on* 17.3 (2002): 392-399.
5. Dorrell, David G., William T. Thomson, and Steven Roach. Analysis of airgap flux, current, and vibration signals as a function of the combination of static and dynamic airgap eccentricity in 3-phase induction motors. *Industry Applications, IEEE Transactions on* 33.1 (1997): 24-34.
6. Devaney, Michael J., and Levent Eren. Detecting motor bearing faults. *Instrumentation & Measurement Magazine, IEEE* 7.4 (2004): 30-50.
7. Riley, Caryn M., et al. Stator current harmonics and their causal vibrations: a preliminary investigation of sensorless vibration monitoring applications. *Industry Applications, IEEE Transactions on* 35.1 (1999): 94-99.
8. Singh, G. K., and Ahmed Saleh Al Kazzaz. Induction machine drive condition monitoring and diagnostic research—a survey. *Electric Power Systems Research* 64.2 (2003): 145-158.
9. Briz, Fernando, et al. Online diagnostics in inverter-fed induction machines using high-frequency signal injection. *Industry Applications, IEEE Transactions on* 40.4 (2004): 1153-1161.
10. Akin, Bilal, et al. A simple real-time fault signature monitoring tool for motor-drive-embedded fault diagnosis systems. *Industrial Electronics, IEEE Transactions on* 58.5 (2011): 1990-2001.
11. Kim, Byunghwan, et al. Automated detection of rotor faults for inverter-fed induction machines under standstill conditions. *Industry Applications, IEEE Transactions on* 47.1 (2011): 55-64.

- 744 12. Gupta, R. A., A. K. Wadhwani, and S. R. Kapoor. Early estimation of faults in induction
745 motors using symbolic dynamic-based analysis of stator current samples. *Energy*
746 *Conversion, IEEE Transactions on* 26.1 (2011): 102-114.
- 747 13. Arthur, Neil, and Jim Penman. Induction machine condition monitoring with higher order
748 spectra. *Industrial Electronics, IEEE Transactions on* 47.5 (2000): 1031-1041.
- 749 14. Bellini, Alberto, Giovanni Franceschini, and Carla Tassoni. Monitoring of induction
750 machines by maximum covariance method for frequency tracking. *Industry Applications,*
751 *IEEE Transactions on* 42.1 (2006): 69-78.
- 752 15. Peng, Z. K., Peter W. Tse, and F. L. Chu. A comparison study of improved Hilbert–
753 Huang transform and wavelet transform: application to fault diagnosis for rolling bearing.
754 *Mechanical systems and signal processing* 19.5 (2005): 974-988.
- 755 16. Purushotham, V., S. Narayanan, and Suryanarayana AN Prasad. Multi-fault diagnosis of
756 rolling bearing elements using wavelet analysis and hidden Markov model based fault
757 recognition. *NDT & E International* 38.8 (2005): 654-664.
- 758 17. Bruzzese, Claudio. Analysis and application of particular current signatures (symptoms)
759 for cage monitoring in nonsinusoidally fed motors with high rejection to drive load, inertia,
760 and frequency variations. *Industrial Electronics, IEEE Transactions on* 55.12 (2008): 4137-
761 4155.
- 762 18. Bellini, Alberto, et al. On-field experience with online diagnosis of large induction motors
763 cage failures using MCSA. *Industry Applications, IEEE Transactions on* 38.4 (2002): 1045-
764 1053.
- 765 19. Wang, KeSheng. *Vibration monitoring on electrical machine using Vold-Kalman filter*
766 *order tracking*. Diss. University of Pretoria, 2008.
- 767 20. Bellini, Alberto, et al. Advances in diagnostic techniques for induction machines.
768 *Industrial Electronics, IEEE Transactions on* 55.12 (2008): 4109-4126.
- 769 21. Bellini, Alberto, et al. Closed-loop control impact on the diagnosis of induction motors
770 faults. *Industry Applications, IEEE Transactions on* 36.5 (2000): 1318-1329.
- 771 22. Cruz, S. M. A., and A. J. M. Cardoso. Diagnosis of rotor faults in closed-loop induction
772 motor drives. *Industry Applications Conference, 2006. 41st IAS Annual Meeting. Conference*
773 *Record of the 2006 IEEE*. Vol. 5. IEEE, 2006.
- 774 23. Cruz, Sérgio MA, et al. A new model-based technique for the diagnosis of rotor faults in
775 RFOC induction motor drives. *Industrial Electronics, IEEE Transactions on* 55.12 (2008):
776 4218-4228.
- 777 24. Jung, Jee-Hoon, Jong-Jae Lee, and Bong-Hwan Kwon. Online diagnosis of induction
778 motors using MCSA. *Industrial Electronics, IEEE Transactions on* 53.6 (2006): 1842-1852.

- 779 25. Szabo, L., et al. An Overview on Induction Machine's Diagnosis Methods. *Journal of*
780 *Computer Science and Control Systems* 1 (2008).
- 781 26. Gilreath, Phil, and Brij N. Singh. A new centroid based fault detection method for 3-
782 phase inverter-fed induction motors. *Power Electronics Specialists Conference, 2005.*
783 *PESC'05. IEEE 36th.* IEEE, 2005.
- 784 27. Tu, Xiaoping, et al. Modeling and real-time simulation of internal faults in synchronous
785 generators with parallel-connected windings. *Industrial Electronics, IEEE Transactions*
786 *on* 54.3 (2007): 1400-1409.
- 787 28. Cruz, Sergio MA, and AJ Marques Cardoso. Multiple reference frames theory: A new
788 method for the diagnosis of stator faults in three-phase induction motors. *Energy*
789 *Conversion, IEEE Transactions on* 20.3 (2005): 611-619.
- 790 29. Akin, Bilal, et al. DSP-based sensorless electric motor fault-diagnosis tools for electric
791 and hybrid electric vehicle powertrain applications. *Vehicular Technology, IEEE Transactions*
792 *on* 58.6 (2009): 2679-2688.
- 793 30. Tewari, Diwakar. *Symbolic dynamic models for highly varying power system loads*. Diss.
794 Arizona State University, 2002.
- 795 31. Les Cottrell, R., et al. Evaluation of techniques to detect significant network performance
796 problems using End-to-End active network measurements. *Network Operations and*
797 *Management Symposium, 2006. NOMS 2006. 10th IEEE/IFIP.* IEEE, 2006.
- 798 32. T. W. Kirman, Kolmogorov-Smirnov test at [http://www.physics.csbsju.edu/stats/ks-](http://www.physics.csbsju.edu/stats/ks-test.html)
799 [test.html](http://www.physics.csbsju.edu/stats/ks-test.html) (Tutorial), 1996.
- 800 33. Urresty, J., J. Riba, and Luis Romeral. Diagnosis of Inter-Turn Faults in PMSMs
801 Operating under Non-Stationary Conditions by applying Order Tracking Filtering. *Power*
802 *Electronics, IEEE Transactions on* 28.1 (2013): 507-515.
- 803 34. Vold, Hsvard. High Resolution Order Tracking at Extreme Slew Rates, Using Kalman
804 Tracking Filters. *Shock Vib.*, 2.6 (1995): 507-515.
- 805 35. Peng, Z. K., and F. L. Chu. Application of the wavelet transform in machine condition
806 monitoring and fault diagnostics: a review with bibliography. *Mechanical systems and signal*
807 *processing* 18.2 (2004): 199-221.
- 808 36. Mitoma, Tetsuro, Huaqing Wang, and Peng Chen. Fault diagnosis and condition
809 surveillance for plant rotating machinery using partially-linearized neural network. *Computers*
810 *& Industrial Engineering* 55.4 (2008): 783-794.
- 811 37. Douglas, H., Pragasen Pillay, and A. K. Ziarani. Broken rotor bar detection in induction
812 machines with transient operating speeds. *Energy Conversion, IEEE Transactions on* 20.1
813 (2005): 135-141.

- 814 38. Lebaroud, Abdesselam, and Guy Clerc. Classification of induction machine faults by
815 optimal time–frequency representations. *Industrial Electronics, IEEE Transactions on* 55.12
816 (2008): 4290-4298.
- 817 39. L. Cohen, *Time-Frequency Analysis*. Englewood Cliffs, NJ: Prentice- Hall, 1995.
- 818 40. Wang, Huaqing, and Peng Chen. Fuzzy diagnosis method for rotating machinery in
819 variable rotating speed. *Sensors Journal, IEEE* 11.1 (2011): 23-34.
- 820 41. Wu, Jian-Da, and Chiu-Hong Liu. Investigation of engine fault diagnosis using discrete
821 wavelet transform and neural network. *Expert Systems with Applications* 35.3 (2008): 1200-
822 1213.
- 823 42. Stander, C. J., P. S. Heyns, and W. Schoombie. Using vibration monitoring for local fault
824 detection on gears operating under fluctuating load conditions. *Mechanical Systems and*
825 *Signal Processing* 16.6 (2002): 1005-1024.
- 826 43. Rajagopalan, S., et al. Non-stationary motor fault detection using recent quadratic time-
827 frequency representations. *Industry Applications Conference, 2006. 41st IAS Annual*
828 *Meeting. Conference Record of the 2006 IEEE*. Vol. 5. IEEE, 2006.
- 829 44. Junsheng, Cheng, Yu Dejie, and Yang Yu. Application of an impulse response wavelet to
830 fault diagnosis of rolling bearings. *Mechanical Systems and Signal Processing* 21.2 (2007):
831 920-929.
- 832 45. Wu, Jian-Da, and Chuang-Chin Hsu. Fault gear identification using vibration signal with
833 discrete wavelet transform technique and fuzzy–logic inference. *Expert systems with*
834 *applications* 36.2 (2009): 3785-3794.
- 835 46. Zheng, H., Z. Li, and X. Chen. Gear fault diagnosis based on continuous wavelet
836 transform. *Mechanical systems and signal processing* 16.2 (2002): 447-457.
- 837 47. Zhu, Z. K., et al. Detection of signal transients based on wavelet and statistics for
838 machine fault diagnosis. *Mechanical Systems and Signal Processing* 23.4 (2009): 1076-
839 1097.
- 840 48. Tse, Peter W., Y. H. Peng, and Richard Yam. Wavelet analysis and envelope detection
841 for rolling element bearing fault diagnosis-their effectiveness and flexibilities. *Journal of*
842 *Vibration and Acoustics* 123.3 (2001): 303-310.
- 843 49. Wu, Jian-Da, and Jien-Chen Chen. Continuous wavelet transform technique for fault
844 signal diagnosis of internal combustion engines. *NDT & E International* 39.4 (2006): 304-311.
- 845 50. Staszewski, W. J., K. Worden, and G. R. Tomlinson. Time–frequency analysis in
846 gearbox fault detection using the Wigner–Ville distribution and pattern recognition.
847 *Mechanical systems and signal processing* 11.5 (1997): 673-692.
- 848 51. Meng, Qingfeng, and Liangsheng Qu. Rotating machinery fault diagnosis using Wigner
849 distribution. *Mechanical Systems and Signal Processing* 5.3 (1991): 155-166.

- 850 52. Blodt, Martin, et al. On-line monitoring of mechanical faults in variable-speed induction
851 motor drives using the Wigner distribution. *Industrial Electronics, IEEE Transactions on* 55.2
852 (2008): 522-533.
- 853 53. Cruz, S. M. A., et al. Diagnosis of rotor faults in traction drives for railway applications.
854 *Electrical Machines, 2008. ICEM 2008. 18th International Conference on*. IEEE, 2008.
- 855 54. Legowski, Stanislaw F., A. H. M. Sadrul Ula, and Andrzej M. Trzynadlowski.
856 Instantaneous power as a medium for the signature analysis of induction motors. *Industry*
857 *Applications, IEEE Transactions on* 32.4 (1996): 904-909.
- 858 55. Bellini, Alberto, et al. Quantitative evaluation of induction motor broken bars by means of
859 electrical signature analysis. *Industry Applications, IEEE Transactions on* 37.5 (2001): 1248-
860 1255.
- 861 56. Stone, G. C., et al. Development of automatic, continuous partial discharge monitoring
862 systems to detect motor and generator partial discharges. *Electric Machines and Drives*
863 *Conference Record, 1997. IEEE International*. IEEE, 1997.
- 864 57. *IEEE Trial Use Guide to the Measurement of Partial Discharges in Rotating Machinery*,
865 IEEE 1434-2000.
- 866 58. Tavner, P. J. Review of condition monitoring of rotating electrical machines. *Electric*
867 *Power Applications, IET* 2.4 (2008): 215-247.
- 868 59. Baker, P. C., et al. Development of an integrated low-power RF partial discharge
869 detector. *Electrical Insulation Conference, 2009. EIC 2009. IEEE*. IEEE, 2009.
- 870 60. Tetrault, Serge M., Greg C. Stone, and Howard G. Sedding. Monitoring partial
871 discharges on 4-kV motor windings. *Industry Applications, IEEE Transactions on* 35.3
872 (1999): 682-688.
- 873 61. Stone, Greg, et al. *Electrical insulation for rotating machines: design, evaluation, aging,*
874 *testing, and repair*. Vol. 21. Wiley-IEEE Press, 2004.
- 875 62. Toliyat, Hamid A., and Gerald B. Kliman, eds. *Handbook of electric motors*. Vol. 120.
876 CRC Press, 2010.
- 877 63. Bishop, Tom. Squirrel cage rotor testing. *EASA Convention*. 2003.
- 878 64. Testing of Squirrel Cage Rotors, Elect. App. Serv. Assoc., Inc., St. Louis, MO, EASA
879 Tech. Note 23, 2003.
- 880 65. McKinnon, David L. Using a six fault zone approach for predictive maintenance on
881 motors. *Electrical Insulation Conference and Electrical Manufacturing Expo, 2007*. IEEE,
882 2007.
- 883 66. El Menzhi, L., and A. Saad. Induction motor fault diagnosis using voltage Park
884 components of an auxiliary winding-voltage unbalance. *Electrical Machines and Systems,*
885 *2009. ICEMS 2009. International Conference on*. IEEE, 2009.

- 886 67. El Menzhi, Lamiaa, and Abdallah Saad. Induction motor fault diagnosis using voltage
887 spectrum of an auxiliary winding. *Electrical Machines and Systems, 2007. ICEMS.*
888 *International Conference on.* IEEE, 2007.
- 889 68. Mirimani, Seyyed Mehdi, et al. Static Eccentricity Fault Detection in Single Stator-Single
890 Rotor Axial Flux Permanent Magnet Machines. *Industrial Application, IEEE Transaction on*
891 48.6 (2011): 1-8.
- 892 69. G.G. Acosta, C.J. Verucchi, E.R. Gelso, A current monitoring system for diagnosing
893 electrical failures in induction motors, *Mechanical Systems and Signal Processing* 20 (2006):
894 953–965.
- 895 70. Urresty, J., et al. Detection of demagnetization faults in surface-mounted permanent
896 magnet synchronous motors by means of the zero-sequence voltage component. *Energy*
897 *Conversion, IEEE Transactions on* 27.1 (2012): 42-51.
- 898 71. Urresty, J-C., et al. Detection of inter-turns short circuits in permanent magnet
899 synchronous motors operating under transient conditions by means of the zero sequence
900 voltage. *Power Electronics and Applications (EPE 2011), Proceedings of the 2011-14th*
901 *European Conference on.* IEEE, 2011.
- 902 72. Briz, Fernando, et al. Induction machine diagnostics using zero sequence component.
903 *Industry Applications Conference, 2005. Fourtieth IAS Annual Meeting. Conference Record*
904 *of the 2005.* Vol. 1. IEEE, 2005.
- 905 73. Scheffer, Cornelius, and Paresh Girdhar. *Practical machinery vibration analysis and*
906 *predictive maintenance.* Newnes, 2004.
- 907 74. Han, Y., and Y. H. Song. Condition monitoring techniques for electrical equipment-a
908 literature survey. *Power Delivery, IEEE Transactions on* 18.1 (2003): 4-13.
- 909 75. Rao, J. S. *Vibratory condition monitoring of machines.* CRC Press/ Llc, 2000.
- 910 76. Tavner, Peter J., and James Penman. *Condition monitoring of electrical machines.*
911 Letchworth: Research Studies Press, 1987.
- 912 77. Pöyhönen, S., et al. Numerical magnetic field analysis and signal processing for fault
913 diagnostics of electrical machines. *COMPEL: The International Journal for Computation and*
914 *Mathematics in Electrical and Electronic Engineering* 22.4 (2003): 969-981.
- 915 78. Choi, Seungdeog, et al. Performance-oriented electric motors diagnostics in modern
916 energy conversion systems. *Industrial Electronics, IEEE Transactions on* 59.2 (2012): 1266-
917 1277.
- 918 79. Pineda-Sanchez, M., et al. Diagnosis of induction motor faults in time-varying conditions
919 using the polynomial-phase transform of the current. *Industrial Electronics, IEEE*
920 *Transactions on* 58.4 (2011): 1428-1439.

- 921 80. Yu, Yang, and Cheng Junsheng. A roller bearing fault diagnosis method based on EMD
922 energy entropy and ANN. *Journal of sound and vibration* 294.1 (2006): 269-277.
- 923 81. J. Lin, M. J. Zuo, and K. R. Fyfe. Mechanical fault detection based on the wavelet
924 denoising technique, *Journal of Vibration and Acoustic* 126.1 (2004): 9–16.
- 925 82. Dorrell, David G., William T. Thomson, and Steven Roach. Analysis of airgap flux,
926 current, and vibration signals as a function of the combination of static and dynamic airgap
927 eccentricity in 3-phase induction motors. *Industry Applications, IEEE Transactions on* 33.1
928 (1997): 24-34.
- 929 83. J. Zhuge, Vibration Data Collector Signal Analysis, Part of VDC User's Manual,
930 CRYSTAL instrument, 2009.
- 931 84. Finley, William R., Mark M. Hodowanec, and Warren G. Holter. An analytical approach to
932 solving motor vibration problems. *Petroleum and Chemical Industry Conference, 1999.*
933 *Industry Applications Society 46th Annual.* IEEE, 1999.
- 934 85. Cameron, J. R., W. T. Thomson, and A. B. Dow. Vibration and current monitoring for
935 detecting airgap eccentricity in large induction motors. *IEE Proceedings B (Electric Power*
936 *Applications)*. Vol. 133. No. 3. IET Digital Library, 1986.
- 937 86. Rodríguez, Pedro Vicente Jover, et al. Air-gap force distribution and vibration pattern of
938 induction motors under dynamic eccentricity. *Electrical Engineering* 90.3 (2008): 209-218.
- 939 87. Ellison, A. J., and S. J. Yang. Effects of rotor eccentricity on acoustic noise from
940 induction machines. *Proceedings of the Institution of Electrical Engineers*. Vol. 118. No. 1.
941 IET Digital Library, 1971.
- 942 88. Baydar, Naim, and Andrew Ball. A comparative study of acoustic and vibration signals in
943 detection of gear failures using Wigner–Ville distribution. *Mechanical systems and signal*
944 *processing* 15.6 (2001): 1091-1107.
- 945 89. Scanlon, Patricia, Darren F. Kavanagh, and Francis M. Boland. Residual Life Prediction
946 of Rotating Machines Using Acoustic Noise Signals. (2013): 1-14.
- 947 90. Scanlon, Patricia, Alan M. Lyons, and Alan O'Loughlin. Acoustic signal processing for
948 degradation analysis of rotating machinery to determine the remaining useful life.
949 *Applications of Signal Processing to Audio and Acoustics, 2007 IEEE Workshop on.* IEEE,
950 2007.
- 951 91. Kia, Shahin Hedayati, Humberto Henao, and G-A. Capolino. Mechanical transmission
952 and torsional vibration effects on induction machine stator current and torque in railway
953 traction systems. *Energy Conversion Congress and Exposition, 2009. ECCE 2009. IEEE.*
954 IEEE, 2009.
- 955 92. Holtz, Joachim. Sensorless control of induction motor drives. *Proceedings of the*
956 *IEEE* 90.8 (2002): 1359-1394.

- 957 93. Henao, Humberto, Shahin Hedayati Kia, and G. Capolino. Torsional-vibration
958 assessment and gear-fault diagnosis in railway traction system. *Industrial Electronics, IEEE*
959 *Transactions on* 58.5 (2011): 1707-1717.
- 960 94. Guzinski, Jaroslaw, et al. Application of speed and load torque observers in high-speed
961 train drive for diagnostic purposes. *Industrial Electronics, IEEE Transactions on* 56.1 (2009):
962 248-256.
- 963 95. Mehala, N. E. E. L. A. M. Condition monitoring and fault diagnosis of induction motor
964 using motor current signature analysis. *Doctor of philosophy, Electrical Engineering, National*
965 *Institute of Technology Kurukshetra, India October*(2010).
- 966 96. Hsu, John S. Monitoring of defects in induction motors through air-gap torque
967 observation. *Industry Applications, IEEE Transactions on* 31.5 (1995): 1016-1021.
- 968 97. R. Maier. Protection of squirrel-cage induction motors using instantaneous power and
969 phase application. *Industry Application s, IEEE Transaction on* 28.2 (1992): 376–380.
- 970 98. Motor and Generators, NEMA Standard Publication No.MG 1- 1998 (Revision 2-2001).
- 971 99. Carson, C. C., S. C. Barton, and F. S. Echeverria. Immediate Warning of Local
972 Overheating in Electric Machines by the Detection of Pyrolysis Products. *Power Apparatus*
973 *and Systems, IEEE Transactions on* 2 (1973): 533-542.
- 974 100. Hongbo, Fan, et al. Study on oil detection technology based on inductive wear debris
975 sensor. *Electronic Measurement & Instruments, 2009. ICEMI'09. 9th International*
976 *Conference on*. IEEE, 2009.
- 977 101. Xufeng, Jiang, et al. Study on Aero-engine Wear Fault Diagnosis by Direct Reading
978 Ferrograph. *Measuring Technology and Mechatronics Automation (ICMTMA), 2011 Third*
979 *International Conference on*. Vol. 3. IEEE, 2011.
- 980 102. Laghari, M. S., F. Ahmed, and J. Aziz. Wear particle shape and edge detail analysis.
981 *Computer and Automation Engineering (ICCAE), 2010 The 2nd International Conference on*.
982 Vol. 1. IEEE, 2010.
- 983 103. Milic, Saša D., and Milesa Z. Sreckovic. A stationary system of noncontact temperature
984 measurement and hotbox detecting. *Vehicular Technology, IEEE Transactions on* 57.5
985 (2008): 2684-2694.
- 986 104. Boglietti, Aldo, et al. Evolution and modern approaches for thermal analysis of electrical
987 machines. *Industrial Electronics, IEEE Transactions on* 56.3 (2009): 871-882.
- 988 105. Mellor, P. H., D. Roberts, and D. R. Turner. Lumped parameter thermal model for
989 electrical machines of TEFC design. *IEE Proceedings B (Electric Power Applications)*. Vol.
990 138. No. 5. IET Digital Library, 1991.

- 991 106. Okoro, Ogbonnaya I. Steady and transient states thermal analysis of a 7.5-kW squirrel-
992 cage induction machine at rated-load operation. *Energy Conversion, IEEE Transactions*
993 *on* 20.4 (2005): 730-736.
- 994 107. Nerg, Janne, Marko Rilla, and Juha Pyrhonen. Thermal analysis of radial-flux electrical
995 machines with a high power density. *Industrial Electronics, IEEE Transactions on* 55.10
996 (2008): 3543-3554.
- 997 108. Chowdhury, S. K., and P. K. Baski. A simple lumped parameter thermal model for
998 electrical machine of TEFC design. *Power Electronics, Drives and Energy Systems (PEDES)*
999 *& 2010 Power India, 2010 Joint International Conference on*. IEEE, 2010.
- 1000 109. Gao, Zhi, Thomas G. Habetler, and Ronald G. Harley. An online adaptive stator winding
1001 temperature estimator based on a hybrid thermal model for induction machines. *Electric*
1002 *Machines and Drives, 2005 IEEE International Conference on*. IEEE, 2005.
- 1003 110. Moreno, J. Fernández, F. Pérez Hidalgo, and M. D. Martinez. Realisation of tests to
1004 determine the parameters of the thermal model of an induction machine. *Electric Power*
1005 *Applications, IEE Proceedings-*. Vol. 148. No. 5. IET, 2001.
- 1006 111. Milanfar, Peyman, and Jeffrey H. Lang. Monitoring the thermal condition of permanent-
1007 magnet synchronous motors. *Aerospace and Electronic Systems, IEEE Transactions*
1008 *on* 32.4 (1996): 1421-1429.
- 1009 112. Jankowski, Todd A., et al. Development and validation of a thermal model for electric
1010 induction motors. *Industrial Electronics, IEEE Transactions on* 57.12 (2010): 4043-4054.
- 1011 113. Nategh, Shafigh, et al. Thermal analysis of a PMaSRM using partial FEA and lumped
1012 parameter modeling. *Energy Conversion, IEEE Transactions on* 27.2 (2012): 477-488.
- 1013 114. Kolondzovski, Z., A. Belahcen, and A. Arkkio. Comparative thermal analysis of different
1014 rotor types for a high-speed permanent-magnet electrical machine. *Electric Power*
1015 *Applications, IET* 3.4 (2009): 279-288.
- 1016 115. El-Refaie, Ayman M., et al. Thermal analysis of multibarrier interior PM synchronous
1017 machine using lumped parameter model. *Energy Conversion, IEEE Transactions on* 19.2
1018 (2004): 303-309.
- 1019 116. Idoughi, Laïd, et al. Thermal model with winding homogenization and FIT discretization
1020 for stator slot. *Magnetics, IEEE Transactions on* 47.12 (2011): 4822-4826.
- 1021 117. Lipo, Thomas A. *Vector control and dynamics of AC drives*. Vol. 41. Oxford University
1022 Press, USA, 1996.
- 1023 118. Lee, Sang-Bin, et al. A stator and rotor resistance estimation technique for conductor
1024 temperature monitoring. *Industry Applications Conference, 2000. Conference Record of the*
1025 *2000 IEEE*. Vol. 1. IEEE, 2000.

- 1026 119. Zhang, Pinjia, et al. A DC signal injection-based thermal protection scheme for soft-
1027 starter-connected induction motors. *Industry Applications, IEEE Transactions on* 45.4
1028 (2009): 1351-1358.
- 1029 120. Zhang, Pinjia, Bin Lu, and Thomas G. Habetler. A remote and sensorless stator winding
1030 resistance estimation method for thermal protection of soft-starter-connected induction
1031 machines. *Industrial Electronics, IEEE Transactions on* 55.10 (2008): 3611-3618.
- 1032 121. Cheng, Siwei, et al. A nonintrusive thermal monitoring method for closed-loop drive-fed
1033 induction machines. *Energy Conversion Congress and Exposition (ECCE), 2011 IEEE*.
1034 IEEE, 2011.
- 1035 122. Samanta, B., and C. Nataraj. Use of particle swarm optimization for machinery fault
1036 detection. *Engineering Applications of Artificial Intelligence* 22.2 (2009): 308-316.
- 1037 123. Nejari, Hamid, and Mohamed El Hachemi Benbouzid. Monitoring and diagnosis of
1038 induction motors electrical faults using a current Park's vector pattern learning approach.
1039 *Industry Applications, IEEE Transactions on* 36.3 (2000): 730-735.
- 1040 124. Wang, Huaqing, and Peng Chen. Sequential fuzzy diagnosis for condition monitoring of
1041 rolling bearing based on neural network. *Advances in Neural Networks-ISNN 2008*. Springer
1042 Berlin Heidelberg, 2008. 284-293.
- 1043 125. Tag Eldin, E. M., et al. Monitoring and diagnosis of external faults in three phase
1044 induction motors using artificial neural network. *Power Engineering Society General Meeting*,
1045 2007. IEEE. IEEE, 2007.
- 1046 126. Asiri, Yahya, et al. Neural network based classification of partial discharge in HV
1047 motors. *Electrical Insulation Conference (EIC), 2011*. IEEE, 2011.
- 1048 127. Raj, Santhana, and N. Murali. Early classification of bearing faults using morphological
1049 operators and fuzzy inference. *Industrial Electronics, IEEE Transaction on* 60.2 (2013): 567-
1050 574.
- 1051 128. Chandra Sekhar, S., and T. V. Sreenivas. Adaptive spectrogram vs. adaptive pseudo-
1052 Wigner–Ville distribution for instantaneous frequency estimation. *Signal Processing* 83.7
1053 (2003): 1529-1543.
- 1054 129. Cayrac, Didier, Didier Dubois, and Henri Prade. Handling uncertainty with possibility
1055 theory and fuzzy sets in a satellite fault diagnosis application. *Fuzzy Systems, IEEE*
1056 *Transactions on* 4.3 (1996): 251-269.
- 1057 130. Li, Ke, Peng Chen, and Shiming Wang. An Intelligent diagnosis method for rotating
1058 machinery using least squares mapping and a fuzzy neural network. *Sensors* 12.5 (2012):
1059 5919-5939.
- 1060 131. Yazidi, Amine, et al. A web-based remote laboratory for monitoring and diagnosis of ac
1061 electrical machines. *Industrial Electronics, IEEE Transactions on* 58.10 (2011): 4950-4959.

- 1062 132. Yazici, Birsen, and Gerald B. Kliman. An adaptive statistical time-frequency method for
1063 detection of broken bars and bearing faults in motors using stator current. *Industry*
1064 *Applications, IEEE Transactions on* 35.2 (1999): 442-452.
- 1065 133. Ocak, Hasan. *Fault detection, diagnosis and prognosis of rolling element bearings:*
1066 *Frequency domain methods and hidden markov modeling*. Diss. Case Western Reserve
1067 University, 2004.
- 1068 134. M. Blodt, D. Bonacci, J. Regnier, M. Chabret and J. Faucher. On-line monitoring of
1069 mechanical faults in variable-speed induction motor drives using the Winger distribution.
1070 *Industrial Electronics. IEEE Transaction on* 55.2 (2008): 522-533.
- 1071
1072