

Original Research Article**COMBINED EFFECTS OF HALL CURRENT AND MAGNETIC FIELD ON
UNSTEADY FLOW PAST SEMI-INFINITE VERTICAL PLATE WITH
THERMAL RADIATION AND HEAT SOURCE****Abstract**

In the present study combined effects of Hall current and magnetic field on unsteady laminar boundary layer flow of a chemically reacting incompressible viscous fluid along a semi-infinite vertical plate with thermal radiation and heat source is analyzed numerically. A magnetic field of uniform strength is applied normal to the flow. Viscous dissipation and thermal diffusion effects are included. In order to establish a finite boundary condition ($\eta \rightarrow 1$) instead of an infinite plate condition, the governing equations in non-dimensional form are transformed to new system of co-ordinates. Obtaining exact solution for this new system of differential equations is very difficult due to its coupled non-linearity, so they are transformed to system of linear equations using implicit finite difference formulae and these are solved using 'Gaussian elimination' method and for this simulation is carried out by coding in C-Program. Graphical results for velocity, temperature and concentration fields are presented and discussed. The results obtained for skin-friction coefficient, Nusselt and Sherwood numbers are discussed and compared with previously published work in the absence of Hall current parameter. These comparisons have shown a good agreement between the results. A research finding of this study, achieved that the velocity and temperature profiles are severely affected by the Hall effect and magnetic field and also a considerable enhancement in temperature, main and secondary flow velocities of the fluid is observed for increasing values of radiation parameter.

Key words:

Hall current, magnetic field, radiative heat flux, chemical reaction, Implicit finite difference method,

1. Introduction

33 Considerable attention has been given to the unsteady free-convection flow of viscous
 34 incompressible, electrically conducting fluid in the presence of applied magnetic field
 35 in connection with the theory of fluid motion in the liquid core of the earth,
 36 meteorological and oceanographic applications. Due to the gyration and drift of
 37 charged particles, the conductivity parallel to the electric field is reduced and the
 38 current is induced in the direction normal to both electric and magnetic fields. This
 39 phenomenon is known as the 'Hall effect'. This effect on the fluid flow with variable
 40 concentration has a lot of applications in MHD power generators, general
 41 astrophysical and meteorological studies and it can be taken into account within the
 42 range of magneto hydro dynamical approximations. Hiroshi sato [1] has studied the
 43 effect of Hall current on the steady hydro magnetic flow between two parallel plates.
 44 Masakazu katagiri [2] studied the steady incompressible boundary layer flow past a
 45 semi infinite flat plate in a transverse magnetic field at small magnetic Reynolds
 46 number considering with the effect of Hall current. On the other hand Hossain [3]
 47 studied the unsteady flow of incompressible fluid along an infinite vertical porous flat
 48 plate subjected to suction/injection velocity proportional to $(\text{time})^{-1/2}$. Hossain *et al* [4]
 49 investigated the effect of Hall current on the unsteady free convection flow of a
 50 viscous incompressible fluid with mass transfer along a vertical porous plate subjected
 51 to a time dependent transpiration velocity when the constant magnetic field is applied
 52 normal to the flow. Srigopal Agarwal [5] discussed the effect of hall current on the
 53 unsteady hydro magnetic flow of viscous stratified fluid through a porous medium in
 54 the free convection currents. Ajay kumar singh [6] analyzed the steady MHD free
 55 convection and mass transfer flow with Hall current, viscous dissipation and joule
 56 heating, taking in to account the thermal diffusion effect. In all these studies, the effect
 57 of Hall current with radiation on the flow field has not been discussed.

58

59 Several authors have dealt with heat flow and mass transfer over a vertical porous
 60 plate with variable suction, heat absorption/ generation, radiation and chemical
 61 reaction. Actually many process in engineering areas occur at high temperature and
 62 knowledge of radiation heat transfer becomes very important for the design of the
 63 pertinent equipment. Nuclear power plants, gas turbines and the various propulsion

64 devices for air craft, missiles, satellites and space vehicles are examples of such
65 engineering areas. In such cases one has to take into account the effects of radiation.
66 So, Perdikis and Raptis [7] illustrated the heat transfer of a micro polar fluid in the
67 presence of radiation. Takhar 'et al.' [8] considered the effects of radiation on free-
68 convection flow of a radiation gas past a semi infinite vertical plate in the presence of
69 magnetic field. Raptis and Massalas [9] studied the magneto-hydrodynamic flow past
70 a plate by the presence of radiation. Elbashbeshby and Bazid [10] have reported the
71 effect of radiation on forced convection flow of a micro polar fluid over a horizontal
72 plate. Chamka et al. [11] studied the effect of radiation on free convection flow past a
73 semi infinite vertical plate with mass transfer. Ganeshan and Loganathan[12] analyzed
74 the radiation and mass transfer effects on flow of an incompressible viscous fluid past
75 a moving cylinder. Kim et al. [13] analyzed the effect of radiation on transient mixed
76 convection flow of a micropolar fluid past a moving semi infinite vertical porous
77 plate. Makinde [14] examined the transient free convection interaction with thermal
78 radiation of an absorbing-emitting fluid. Perdikis and Rapti [15] discussed unsteady
79 magnetic hydrodynamic flow in the presence of radiation.

80
81 Ramachandra prasad et al. [16] considered the effects radiation and mass transfer on
82 two dimensional flow past an infinite vertical plate. Chaudhary and Preethi Jain [17]
83 presented an analysis to study the effects of radiation on the hydromagnetic free
84 convection flow of an electrically conducting micropolar fluid past a vertical porous
85 plate through a porous medium in slip-flow regime. The effect of thermal radiation,
86 time-dependent suction and chemical reaction on the two-dimensional flow of an
87 incompressible Boussinesq fluid, applying a perturbation technique has been studied
88 by Prakash and Ogulu [18]. Later, for this same study a numerical investigation is
89 carried out by Rajireddy and Srihari [19]. Ibrahim 'et al.' [20] analyzed the effects of the
90 chemical reaction and radiation absorption on transient hydro-magnetic free-
91 convection flow past a semi infinite vertical permeable moving plate with wall
92 transpiration and heat source. SudheerBabu and Satyanarayana [21] discussed the
93 effects of the chemical reaction and radiation absorption in the presence of magnetic
94 field on free convection flow through porous medium with variable suction. Dulal Pal

95 'et al.' [22] has made the perturbation analysis to study the effects thermal radiation
 96 and chemical reaction on magneto-hydrodynamic unsteady heat and mass transfer in a
 97 boundary layer flow past a vertical permeable plate in the slip flow regime. J. Anand
 98 Rao et al. [23] analyzed the effects of viscous dissipation and Soret on an unsteady
 99 two-dimensional laminar mixed convective boundary layer flow of a chemically
 100 reacting viscous incompressible fluid, along a semi-infinite vertical permeable moving
 101 plate. Recently, Srihari and Kesava Reddy [24] have made the numerical investigation
 102 to study the effects of Soret and magnetic field on unsteady laminar boundary layer
 103 flow of a radiating and chemically reacting incompressible viscous fluid along a semi-
 104 infinite vertical plate. More recently, Srihari and Srinivas Reddy [25] studied the
 105 effects of radiation and Soret number variation in the presence of heat source/sink on
 106 unsteady laminar boundary layer flow of chemically reacting incompressible viscous
 107 fluid along a semi-infinite vertical plate with viscous dissipation.

108

109 In most of the earlier studies analytical or perturbation methods were applied to
 110 obtain the solution of the problem and there seems to be no significant consideration
 111 of the combined effects of Hall current and magnetic field with thermal radiation.
 112 Moreover, when the radiative heat transfer takes place, the fluid involved can be
 113 electrically conducting in the sense that it is ionized owing to the high operating
 114 temperature. Accordingly, it is of interest to examine the effect of magnetic field on
 115 the flow and when the strength of applied magnetic field is strong, one cannot neglect
 116 the effect of Hall current. So in the present study the combined effects of magnetic
 117 field and Hall current on unsteady laminar flow of a chemically reacting
 118 incompressible viscous fluid along a semi-infinite vertical plate with thermal radiation
 119 is investigated. A magnetic field of uniform strength is applied normal to the fluid
 120 flow.

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122 In order to obtain the approximate solution and to describe the physics of the problem,
 123 the present non-linear boundary value problem is solved numerically using implicit
 124 finite difference formulae known as Crank-Nicholson method. The obtained results are
 125 discussed in detail and compared with the results of Skin-friction, Nusselt and Sher-

wood numbers, presented by Srihari and Reddy et al. [22] in the absence of Hall current parameter.

128

129 **2. Formulation of the problem**

130 An unsteady laminar, boundary layer flow of a viscous, incompressible, electrically
131 conducting dissipative and chemically reacting fluid along a semi-infinite vertical
132 plate, with thermal radiation, heat source is considered. The x' -axis taken along the
133 plate in the vertically upward direction and y' -axis normal to it. A magnetic field of
134 uniform strength applied along y' -axis. Further, due to the semi-infinite plane surface
135 assumption, the flow variables are functions of normal distance y' and t' only. A time
136 dependent suction velocity is assumed normal to the plate. A magnetic field of
137 uniform strength is assumed to be applied transversely to the porous plate. The
138 magnetic Reynolds number of the flow is taken to be small enough so that the induced
139 magnetic field can be neglected. The equation of conservation of electric
140 charge $\nabla \cdot \vec{J} = 0$, gives $j_y = \text{constant}$, where $\vec{J} = (j_x, j_y, j_z)$. We further assume that the
141 plate is non-conducting. This implies $j_y = 0$ at the plate and hence zero everywhere.
142 When the strength of magnetic field is very large the generalized Ohm's law, in the
143 absence of electric field takes the following form:

144

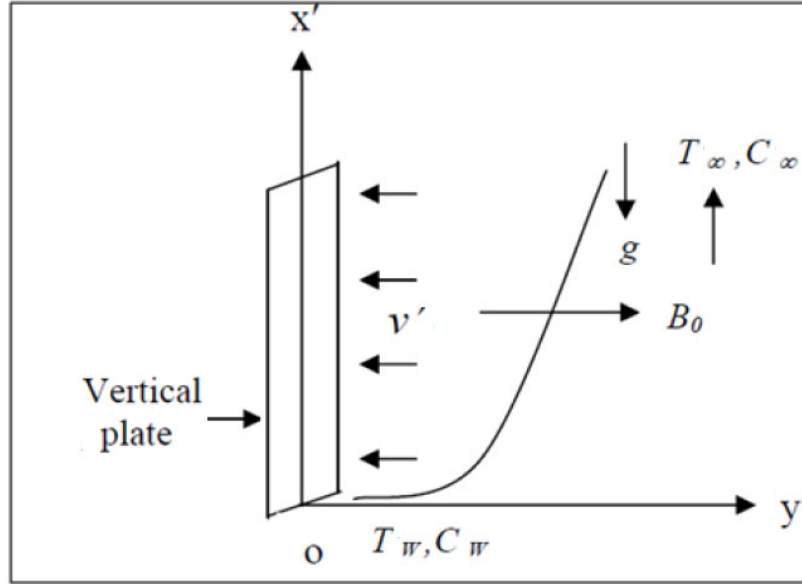
$$145 \quad \vec{J} + \frac{\omega_e \tau_e}{B_0} (\vec{J} \times \vec{B}) = \sigma \left(\vec{V} \times \vec{B} + \frac{1}{en_e} \nabla P_e \right) \quad (1)$$

146 Where \vec{V} is the velocity vector, σ is the electric conductivity, ω_e is the electron
147 frequency, τ_e is the electron collision time, e is the electron charge, n_e is the number
148 density of the electron and P_e is the electron pressure. Under the assumption that the
149 electron pressure (for weakly ionized gas), the thermo-electric pressure and ion-slip
150 are negligible, equation (2.1) becomes:

151

$$152 \quad J_x = \frac{\sigma B_0}{1+m^2} (mu - w) \text{ and } j_z = \frac{\sigma B_0}{1+m^2} (u + mw) \quad (2)$$

153 where u is the x -component of V , w is the z component of V and $m(=w_e\tau_e)$ is the
 154 Hall parameter.
 155



156
 157
 158 **Fig 2.1: Schematic diagram of flow geometry**

159
 160 Within the above framework, the equations which govern the flow under the usual
 161 Boussinesq approximation are as follows:

162
 163 • **Continuity**

164
$$\frac{\partial v'}{\partial y'} = 0 \quad (3)$$

165
 166 • **Momentum equations**

167
 168
$$\frac{\partial u'}{\partial t'} + v' \frac{\partial u'}{\partial y'} = \nu \frac{\partial^2 u'}{\partial y'^2} + g\beta(T - T_\infty) + g\beta^*(C - C_\infty) - \frac{\sigma B_0^2}{\rho(1+m^2)}(u' + mw') \quad (4)$$

169
 170
$$\frac{\partial w'}{\partial t'} + v' \frac{\partial w'}{\partial y'} = \nu \frac{\partial^2 w'}{\partial y'^2} - \frac{\sigma B_0^2}{\rho(1+m^2)}(w' - mu') \quad (5)$$

171

172 • **Energy**

$$173 \quad \frac{\partial T}{\partial t'} + v' \frac{\partial T}{\partial y'} = \frac{k}{\rho C_p} \frac{\partial^2 T}{\partial y'^2} - \frac{1}{\rho c_p} \frac{\partial q_r}{\partial y'} + \frac{\mu}{\rho c_p} \left(\frac{\partial u'}{\partial y'} \right)^2 + \frac{Q(T - T_\infty)}{\rho c_p} \quad (6)$$

174

175 • **Mass transfer**

$$176 \quad \frac{\partial C}{\partial t'} + v' \frac{\partial C}{\partial y'} = D \frac{\partial^2 C}{\partial y'^2} + \frac{D_m k_T}{T_m} \frac{\partial^2 T}{\partial y'^2} - k_r^2 C \quad (7)$$

177

178 The radiative flux q_r by using the Rosseland approximation [26], is given by

179

$$180 \quad q_r = -\frac{4\sigma^*}{3a_R} \frac{\partial T^4}{\partial y'} \quad (8)$$

181 The boundary conditions suggested by the physics of the problem are

$$u' = U_0, w' = 0, T = T_w + \varepsilon(T_w - T_\infty)e^{n't'}, C = C_w + \varepsilon(C_w - C_\infty)e^{n't'} \quad \text{at } y' = 0$$

$$182 \quad u' \rightarrow 0, w' = 0, T \rightarrow T_\infty, C \rightarrow C_\infty \quad \text{as } y' \rightarrow \infty \quad (9)$$

183 It has been assumed that the temperature differences within the flow are sufficiently
184 small and T^4 may be expressed as a linear function of the temperature T . This is
185 accomplished by expanding T^4 in a Taylor series about T_∞ and neglecting higher order
186 terms, we have [26]

$$187 \quad T^4 \approx 4T_\infty^3 T - 3T_\infty^4 \quad (10)$$

188 Using (10) in (8) and then (8) in (6), it implies

189

$$190 \quad \frac{\partial T}{\partial t'} + v' \frac{\partial T}{\partial y'} = \frac{k}{\rho c_p} \frac{\partial^2 T}{\partial y'^2} - \frac{16\sigma^* T_\infty^3}{3\rho c_p k^*} \frac{\partial^2 T}{\partial y'^2} + \frac{\mu}{\rho c_p} \left(\frac{\partial u'}{\partial y'} \right)^2 + \frac{Q(T - T_\infty)}{\rho c_p} \quad (11)$$

191

192 Integration of continuity eqn (1) for variable suction velocity normal to the plate gives

$$193 \quad v' = -U_0(1 + \varepsilon A e^{n't'}) \quad (12)$$

194 where A is the suction parameter and εA is less than unity. Here U_0 is mean suction
195 velocity, which is a non-zero positive constant and the minus sign indicates that the
196 suction is towards the plate.

197 In order to obtain the non-dimensional partial differential equations and with boundary
198 conditions, introducing the following non-dimensional quantities

199

$$200 \quad u = \frac{u'}{U_0}, \quad w = \frac{w'}{U_0}, \quad y = \frac{y'U_0}{\nu}, \quad t = \frac{U_0^2 t'}{\nu}, \quad \theta = \frac{T - T_\infty}{T_w - T_\infty},$$

$$201 \quad \phi = \frac{C - C_\infty}{C_w - C_\infty}, \quad \text{Pr} = \frac{\mu C_p}{k}, \quad \text{Sc} = \frac{\nu}{D}, \quad M = \frac{\sigma B_0^2 \nu}{\rho U_0^2}, \quad \text{So} = \frac{D_m k_T (T_w - T_\infty)}{\nu T_m (C_w - C_\infty)}$$

$$202 \quad \text{Gr} = \frac{g\beta\nu(T_w - T_\infty)}{U_0^3}, \quad \text{Gm} = \frac{g\beta^*\nu(C_w - C_\infty)}{U_0^3}, \quad S = \frac{Q\nu}{\rho C_p U_0^2} \quad (13)$$

203

$$204 \quad \text{Kr} = \frac{k_r'^2 \nu}{U_0^2}, \quad \text{NR} = \frac{16\sigma^* T_\infty^3}{3ka_R}, \quad \text{Ec} = \frac{U_0^2}{C_p (T_w - T_\infty)}, \quad n = \frac{\nu n'}{U_0^2}, \text{ in to equations (4), (5),}$$

205 (7) and (11), we get

$$206 \quad \frac{\partial u}{\partial t} - (1 + \varepsilon A e^{nt}) \frac{\partial u}{\partial y} = \frac{\partial^2 u}{\partial y^2} - \frac{M}{1+m^2} (u + mw) + \text{Gr}\theta + \text{Gm}\phi \quad (14)$$

$$207 \quad \frac{\partial w}{\partial t} - (1 + \varepsilon A e^{nt}) \frac{\partial w}{\partial y} = \frac{\partial^2 w}{\partial y^2} - \frac{M}{1+m^2} (w - mu) \quad (15)$$

$$208 \quad \frac{\partial \theta}{\partial t} - (1 + \varepsilon A e^{nt}) \frac{\partial \theta}{\partial y} = \left(\frac{1 + \text{NR}}{\text{Pr}} \right) \frac{\partial^2 \theta}{\partial y^2} + \text{Ec} \left(\frac{\partial u}{\partial y} \right)^2 + S\theta \quad (16)$$

$$209 \quad \frac{\partial \phi}{\partial t} - (1 + \varepsilon A e^{nt}) \frac{\partial \phi}{\partial y} = \frac{1}{\text{Sc}} \frac{\partial^2 \phi}{\partial y^2} + \text{So} \frac{\partial^2 \theta}{\partial y^2} - \text{Kr}\phi \quad (17)$$

210

211 with the boundary conditions

$$212 \quad u = 1, \quad w = 0, \quad \theta = 1 + \varepsilon e^{nt}, \quad \phi = 1 + \varepsilon e^{nt} \quad \text{at } y = 0$$

$$213 \quad u \rightarrow 0, \quad w = 0, \quad \theta \rightarrow 0, \quad \phi \rightarrow 0 \quad \text{as } y \rightarrow \infty \quad (18)$$

214

215 In order to establish a finite plate condition, $\eta \rightarrow 1$ in equation (18) instead of an
216 infinite boundary condition, $y \rightarrow \infty$, employing the transformation $\eta = 1 - e^{-y}$ on
217 equations (14)-(18), we get

218

$$219 \quad \frac{\partial u}{\partial t} - (1 + \varepsilon A e^{nt})(1 - \eta) \frac{\partial u}{\partial \eta} = (1 - \eta)^2 \frac{\partial^2 u}{\partial \eta^2} - (1 - \eta) \frac{\partial u}{\partial \eta} - \frac{M}{1 + m^2} (u + mw) + Gr\theta + Gm\phi$$

$$220 \quad (19)$$

$$221 \quad \frac{\partial w}{\partial t} - (1 + \varepsilon A e^{nt})(1 - \eta) \frac{\partial w}{\partial \eta} = (1 - \eta)^2 \frac{\partial^2 w}{\partial \eta^2} - (1 - \eta) \frac{\partial w}{\partial \eta} - \frac{M}{1 + m^2} (w - mu) \quad (20)$$

$$222 \quad \frac{\partial \theta}{\partial t} - (1 + \varepsilon A e^{nt})(1 - \eta) \frac{\partial \theta}{\partial \eta} = \left(\frac{1 + NR}{Pr} \right) \left((1 - \eta)^2 \frac{\partial^2 \theta}{\partial \eta^2} - (1 - \eta) \frac{\partial \theta}{\partial \eta} \right) + Ec \left((1 - \eta) \frac{\partial u}{\partial \eta} \right)^2 + S\theta$$

$$223 \quad (21)$$

$$224 \quad \frac{\partial \phi}{\partial t} - (1 + \varepsilon A e^{nt})(1 - \eta) \frac{\partial \phi}{\partial \eta} = \frac{1}{Sc} \left((1 - \eta)^2 \frac{\partial^2 \phi}{\partial \eta^2} - (1 - \eta) \frac{\partial \phi}{\partial \eta} \right) +$$

$$So \left((1 - \eta)^2 \frac{\partial^2 \theta}{\partial \eta^2} - (1 - \eta) \frac{\partial \theta}{\partial \eta} \right) - Kr\phi \quad (22)$$

225 with boundary conditions

226

$$227 \quad u = 1: w = 0, \theta = 1 + \varepsilon e^{nt}, \phi = 1 + \varepsilon e^{nt} \quad \text{at } \eta = 0$$

$$u \rightarrow 0: w = 0, \theta \rightarrow 0, \phi \rightarrow 1 + \varepsilon e^{nt} \quad \text{as } \eta \rightarrow 1$$

$$228 \quad (23)$$

229 3. Method of solution

230 Equations (19)-(22) are non-linear coupled, differential equations, for which obtaining
 231 exact solution is very difficult, so they are transformed to system of linear equations
 232 using implicit finite difference formulae, as follows

$$233 \quad -P_3 r u_{i-1}^{j+1} + (1 + 2P_3 r) u_i^{j+1} - P_3 r u_{i+1}^{j+1} = E_i^j \quad (24)$$

$$234 \quad -P_3 r w_{i-1}^{j+1} + (1 + 2P_3 r) w_i^{j+1} - P_3 r w_{i+1}^{j+1} = D_i^j \quad (25)$$

$$235 \quad -P_3 P_4 r \theta_{i-1}^{j+1} + (1 + 2P_3 P_4 r) \theta_i^{j+1} - P_3 P_4 r \theta_{i+1}^{j+1} = F_i^j \quad (26)$$

236

$$237 \quad -\frac{P_3 r}{Sc} \phi_{i-1}^{j+1} + \left(1 + \frac{2P_3 r}{Sc} \right) \phi_i^{j+1} - \frac{P_3 r}{Sc} \phi_{i+1}^{j+1} = H_i^j \quad (27)$$

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239 with boundary conditions in finite difference form

240

$$\begin{aligned}
 &u(0, j)=1, \quad \theta(0, j)=1+\varepsilon \exp(n . j . k_1), \quad \phi=1+\varepsilon \exp(n . j . k_1), \quad \forall j \\
 &u(10, j) \rightarrow 0, \quad \theta(10, j) \rightarrow 0, \quad \phi(10, j) \rightarrow 1 \quad \forall j
 \end{aligned} \tag{28}$$

where

$$\begin{aligned}
 E_i^j = P_3 r u_{i-1}^j - \left(1 - P_1 P_2 r h - 2 P_3 r + P_2 r h - \frac{M m}{1+m^2} k_1 \right) u_i^j + (P_1 P_2 r h + P_3 r - P_2 r h) u_{i+1}^j \\
 + G r k_1 \theta_i^j + G m k_1 \phi_i^j - \frac{M m}{1+m^2} k_1 w_i^j
 \end{aligned}$$

$$\begin{aligned}
 D_i^j = P_3 r w_{i-1}^j - \left(1 - P_1 P_2 r h - 2 P_3 r + P_2 r h - \frac{M m}{1+m^2} k_1 \right) w_i^j + (P_1 P_2 r h + P_3 r - P_2 r h) w_{i+1}^j \\
 + \frac{M m}{1+m^2} k_1 u_i^j
 \end{aligned}$$

$$F_i^j = P_3 P_4 r \theta_{i-1}^j + (1 - P_1 P_2 r h - 2 P_3 P_4 r + P_2 P_4 r h) \theta_i^j + (P_1 P_2 r h + P_3 P_4 r - P_2 P_4 r h) \theta_{i+1}^j$$

$$\begin{aligned}
 H_i^j = \frac{P_3 r}{S c} \phi_{i-1}^j + \left(1 + P_1 P_2 r h - \frac{2 P_3 r}{S c} + \frac{P_2 r h}{S c} - k_r^2 k_1 \right) \phi_i^j + \left(\frac{P_3 r}{S c} - P_1 P_2 r h - \frac{P_2 r h}{S c} \right) \phi_{i+1}^j \\
 + (2 P_3 r S_0 - S_0 P_1 r h) \theta_{i+1}^j + (S_0 P_1 r h - 4 P_3 r S_0) \theta_i^j + 2 P_3 r S_0 \theta_{i-1}^j
 \end{aligned}$$

$$P_1 = 1 + \varepsilon A e^{n t}, \quad P_2 = 1 - i h, \quad P_3 = \frac{(1 - i h)^2}{2}, \quad P_4 = \frac{1 + N R}{P r},$$

where $r = k_1 / h^2$ and h, k_1 are mesh sizes along η and time direction respectively. Index i refers to space and j for time.

To obtain the difference equations, the region of the flow is divided into a grid or mesh of lines parallel to η and t axes. Solutions of difference equations are obtained at the intersection of these mesh lines called nodes. The finite-difference equations at every internal nodal point on a particular n -level constitute a tri-diagonal system of equations. These equations are solved by Gaussian elimination method and for this a numerical code is executed using C-Program to obtain the approximate solution of the system. In order to prove the convergence of present numerical scheme, the computation is carried out by slightly changed values of h , and k_1 , and the iterations on until a tolerance 10^{-8} is attained. No significant change was observed in the values

of u, w, θ and ϕ . Thus, it is concluded that the finite difference scheme is convergent and stable.

Skin-friction

The Skin friction coefficient τ is given by

$$\tau = \frac{\partial u}{\partial y} \Big|_{y=0} = (1-\eta) \frac{\partial u}{\partial \eta} \Big|_{\eta=0}, \quad (29)$$

Nusselt number

The rate of heat transfer in terms of Nusselt number is given by

$$Nu = \frac{\partial \theta}{\partial y} \Big|_{y=0} = (1-\eta) \frac{\partial \theta}{\partial \eta} \Big|_{\eta=0} \quad (30)$$

Sherwood number

The coefficient of Mass transfer which is generally known as Sherwood number, Sh , is given by

$$Sh = \frac{\partial \phi}{\partial y} \Big|_{y=0} = (1-\eta) \frac{\partial \phi}{\partial \eta} \Big|_{\eta=0} \quad (31)$$

Nomenclature

ρ	Density
C_p	Specific heat at constant pressure
ν	Kinematic viscosity
k	Thermal conductivity
U	Mean velocity
Sc	Schmidt number
T	Temperature
k_r^2	Chemical reaction rate constant

ϵ	Small reference parameter $\ll 1$
Pr	Prandtl number
Gr	Free convection parameter due to temperature
Gm	Free convection parameter due to concentration
m	Hall current
A	Suction parameter
n	A constant exponential index
D	Molar diffusivity
NR	Thermal radiation parameter
β	Coefficient of volumetric thermal expansion of the fluid
β^*	Volumetric coefficient of expansion with concentration
M	Magnetic parameter
σ	Electrical conductivity
ω_e	Electron frequency
τ_e	Electron collision time
e	Electron pressure
n_e	Number density of the electron
P_e	Electron pressure
So	Soret number
Ec	Viscous dissipation

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293 **Table 1 - Effects of Gr, Gm, Pr, Sc, Kr, NR, So and M on Skin-Friction**
 294 **coefficient**
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Gr	Gm	Pr	Sc	Kr	NR	So	M	τ S=0.0, Ec=0.0 Recent[28] (m=0.0)	τ S=2.0, Ec=0.5 More recent [29] (m=0.0)	τ S=2.0, Ec=0.5 Present (m=1.0)
5.0	5.0	0.71	0.24	0.5	0.5	0.0	0.0	1.202	1.4032	1.4032
5.0	5.0	0.71	0.24	0.5	0.5	0.0	2.0	0.557	0.7413	0.98796
5.0	5.0	0.71	0.24	0.5	0.5	2.0	2.0	0.8394	0.9721	1.17426
5.0	5.0	0.71	0.24	0.5	1.0	2.0	2.0	0.9183	1.0523	1.24643
5.0	5.0	0.71	0.6	0.5	0.5	2.0	2.0	0.7601	0.8423	1.01633
5.0	5.0	7.0	0.24	0.5	0.5	2.0	2.0	0.3156	0.3838	0.68666
5.0	<u>10.0</u>	0.71	0.24	0.5	0.5	2.0	2.0	2.6542	2.7352	2.97588
10.0	5.0	0.71	0.24	0.5	0.5	2.0	2.0	2.0447	2.3597	2.58178

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Table 2 - Effects of NR and Pr on Nusselt - number

<i>NR</i>	<i>Pr</i>	<i>Nu</i> S=0.0, Ec=0.0 Recent [28] (m=0.0)	<i>Nu</i> S=2.0, Ec=0.5 More recent [29] (m=0.0)	<i>Nu</i> S=2.0, Ec=0.5 Present (m=1.0)
0.0	0.71	-1.4771	-1.0807	-0.93922
0.5	0.71	- 1.1621	-0.8230	-0.72087
0.5	7.0	- 4.2655	-3.6770	-3.12927
0.5	11.4	-5.3251	-4.7594	-4.03651

Table 3 - Effects of Sc, Kr and So on Sherwood number

<i>Sc</i>	<i>Kr</i>	<i>So</i>	<i>Sh</i> S=0.0, Ec=0.0 Recent [28] (m=0.0)	<i>Sh</i> S=2.0, Ec=0.5 More recent [29] (m=0.0)	<i>Sh</i> S=2.0, Ec=0.5 Present (m=1.0)
0.24	0.5	0.0	-0.5931	-0.59393	-0.59393
0.24	0.5	2.0	-0.1156	-0.37159	-0.37652
0.24	1.0	2.0	-0.1858	-0.43987	-0.44012
0.6	0.5	2.0	-0.00291	-0.55924	-0.56102

326 In order to obtain the approximate solution and to describe the physics of the problem,
 327 in the present work, numerical solution is obtained to study the influence of various
 328 flow parameters encountered in the momentum, energy and mass transfer equations.
 329 To be realistic, the values of Prandtl number (Pr) are chosen to be $Pr = 0.71$ and $Pr =$
 330 7.0 , which represent air and water at temperature 20°C and one atmosphere pressure,
 331 respectively.

332
 333 Figures (1) and (2) show the effect of Hall current (m) on velocity field's u and w
 334 respectively, in the presence of heat source. It is observed that the effect of increasing
 335 values of m results in increasing both the velocity profiles u and w. This due to the
 336 fact that an increase in hall current generates a deflection exerted on moving fluid
 337 causing the level of cross flow velocity maximum and the fluid is dragged further with
 338 more velocity. Furthermore, it is noted that both the velocities u and w increase in the
 339 presence of heat source as the internal heat generation is to increase the rate of heat
 340 transport to the fluid. From figure (3), it is interesting to note that there is a
 341 considerable enhancement in the secondary flow velocity of the fluid is observed for
 342 slightly increasing values of Hall parameter.

343
 344 From figures (4), (5) and (6), it is seen that for increasing values of NR, there is rise in
 345 the temperature, main and cross flow velocities. This due to the fact that an increase in
 346 the value of radiation parameter $NR = 16\sigma^*T_\infty^3/3k a_R$, for given k and T_∞ , leads to
 347 decrease in the Roseland radiation absorbtivity (a_R). According to the equations (6)
 348 and (8), it is concluded that, the divergence of the radiation heat flux ($\partial q_r/\partial y^*$)
 349 increases as a_R decreases and it implies that the rate of radiative heat, transferred to
 350 the fluid increases and consequently the fluid temperature and therefore main and
 351 secondary flow velocities of their particles also increase. Furthermore, it is interested
 352 note that velocity u increases in the presence of radiation.

353
 354 Figures (7) and (8) show the effect magnetic parameter M on main and cross flow
 355 velocity profiles respectively. It is observed from figure (7) that an increase in M leads

356 to decrease in the velocity. This due to the fact that the introduction of transverse magnetic
 357 field in an electrically conducting fluid has a tendency to give rise to a resistive-type force
 358 called the Lorentz force, which acts against the fluid flow and hence results in retarding the
 359 velocity profile. Furthermore, from figure (8) it is seen that for increasing values magnetic
 360 parameter M there is a considerable enhancement in the cross flow velocity w . As the
 361 impact of deflecting force due to the applied magnetic field on the fluid is predominant
 362 rather than main driving cause and therefore a considerable enhancement in the
 363 secondary flow velocity is observed.

364

365 The effect Prandtl number in the presence of heat source parameter on temperature
 366 distribution is shown in figure (9). It is evident from figure that the temperature
 367 increases in the presence of heat source parameter as the effect of internal heat
 368 generation is to increase the rate of heat transport to the fluid. Furthermore it is
 369 interesting to note that with increasing values of Prandtl number Pr , there is a decrease
 370 in the temperature profile. This due to the physical fact that an increase in Pr leads to
 371 decrease in the thermal boundary layer thickness.

372

373 Fig (10) shows the species concentration for different gases like Hydrogen (H_2 :
 374 $Sc=0.22$), Oxygen (O_2 : $Sc=0.66$), Ammonia (NH_3 : $Sc=0.78$) and $Sc = 2.62$ for propyl
 375 benzene at $20^\circ C$ and one atmospheric pressure and for different Kr . It is observed that
 376 the effect of increasing values of chemical reaction parameter and Schmidt number is
 377 to decrease concentration distribution in the flow region.

378

379

380 Results for Skin-friction coefficient, Nusselt and Sherwood numbers are presented in
 381 tables (1), (2) and (3) respectively, in the presence and absence of Hall effect. A
 382 comparative numerical study between present and previous results in tables reveals
 383 that Skin-friction, Nusselt number increase in the presence of Hall current parameter
 384 but Sherwood number decreases slightly in the presence of Hall effect. Further, it is
 385 noted that Skin-friction increases with increasing values of m , NR , Ec , So , Gr and Gm
 386 while it decreases for the increasing values of M , Pr . An increase in Ec , m , S leads to

an increase in the Nusselt number. For increasing values of Sc and Ch decreases the Sherwood number. But it increases with the increasing values So .

In order to access the validity of the present numerical scheme, the present results are compared with previous published data [33] for Skin-friction, rate of heat and mass transfer in the absence of Hall effect. The comparisons in all the cases are found to be in very good agreement and it gives an indication of high degree of coincidence with realistic physical phenomenon.

5. Conclusions:

Combined effects of Hall current and Magnetic field on unsteady laminar flow of a radiating fluid along a semi-infinite vertical plate, with heat source, viscous dissipation and thermal diffusion are analysed. From this study the following conclusions are drawn.

1. The velocity and temperature profiles are severely affected by the magnetic field and Hall effects.
2. For increasing values of Hall current parameters, there is a considerable enhancement in main and secondary flow velocities of the fluid.
3. Magnetic field reduces the main flow velocity profile but there is a considerable enhancement in the cross flow velocity is observed for increasing values same magnetic parameter M .
4. Skin-friction, Nusselt increase in the presence of Hall effect. The temperature, velocity, Skin-friction and Nusselt number increase in the presence heat source
5. There is a rise in the temperature, primary and secondary velocities of the fluid flow for increasing values of radiation parameter.
6. The comparative study, between present and previously published results [33] for Skin-friction, Nusselt and Sherwood numbers in the absence of Hall parameter, shows a good agreement. And therefore it is concluded that the proposed numerical technique, present in the paper is an efficient algorithm with assured convergence.

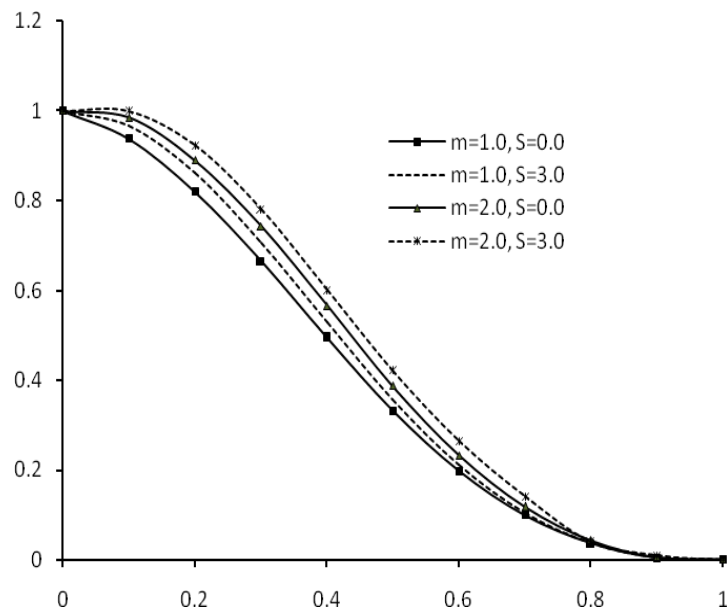


Fig1: Effect of Hall current (m) on velocity field u in the presence of heat source
($Gr=5.0$, $Gm=5.0$, $M=1.0$, $Du=1.0$, $Pr=0.71$, $Ec=0.5$, $NR=0.5$, $Ch=0.5$, $So=1.0$, $Sc=0.22$, $A=0.3$ and $\mathcal{E}=0.01$)

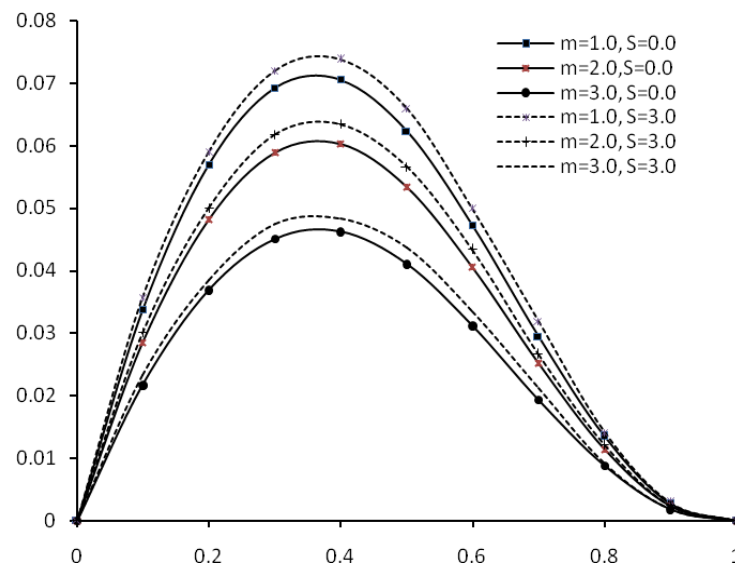


Fig 2: Effect of Hall current (m) on velocity field w in the presence of heat source
($Gr=5.0$, $Gm=5.0$, $M=1.0$, $So=1.0$, $Du=1.0$, $Pr=0.71$, $Ec=0.5$, $NR=0.5$, $Ch=0.5$, $Sc=0.22$, $A=0.3$ and $\mathcal{E}=0.01$)

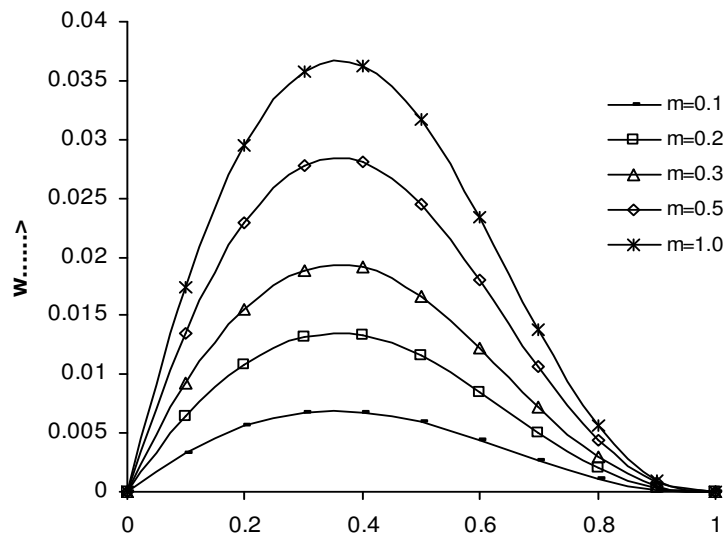


Fig3: Effect of Hall current (m) on velocity component W
(Gr=5.0, Gm=5.0, NR=0.5, Ec=0.2, S=0.5, Pr=0.71, Sc=0.22, Kr=0.5, A=0.3, ε =0.01 and

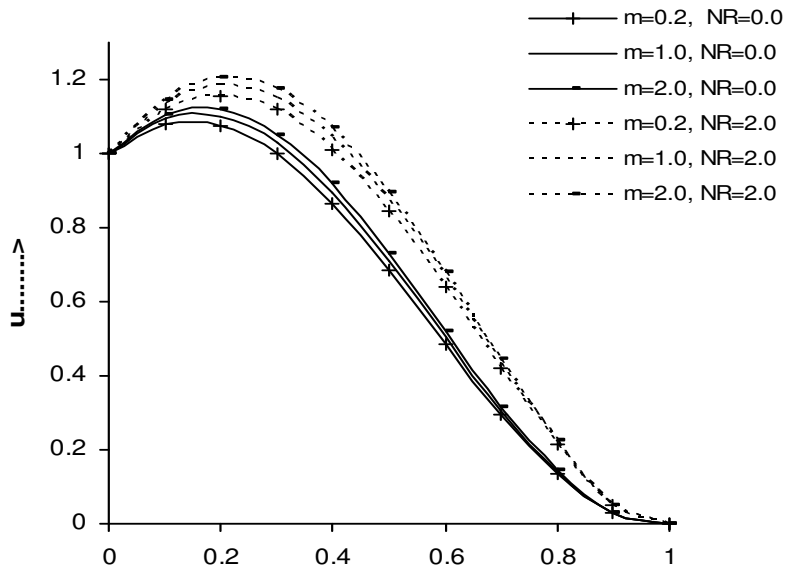


Fig4: Effect of Hall current on velocity field u in the presence/absence of radiation
(Gr=5.0, Gm=5.0, M=1.0, Ec=0.2, S=0.5, Pr=0.71, Sc=0.22, Kr=0.5, A=0.3, ε =0.01 and t=1.0)

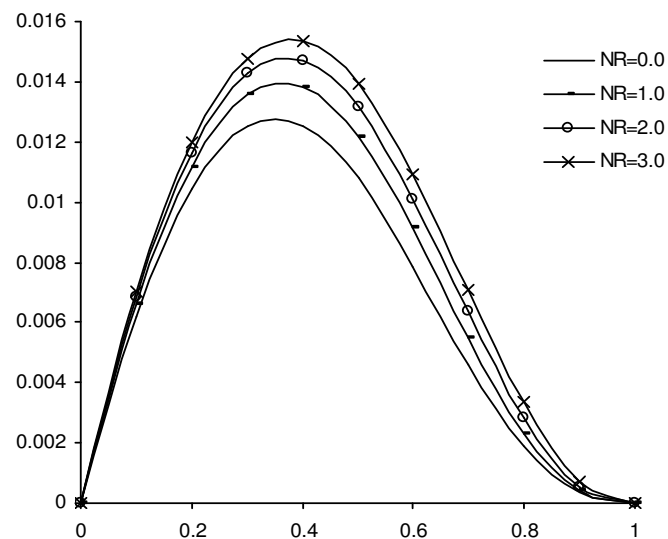


Fig5: Effect of Radiation (NR) on velocity component W
 (Gr=5.0,Gm=5.0,M=1.0,m=0.2,Ec=0.2,S=0.5,Pr=0.71,Sc=0.22,Kr=0.5,A=0.3, \mathcal{E} =0.01 and t=1.0)

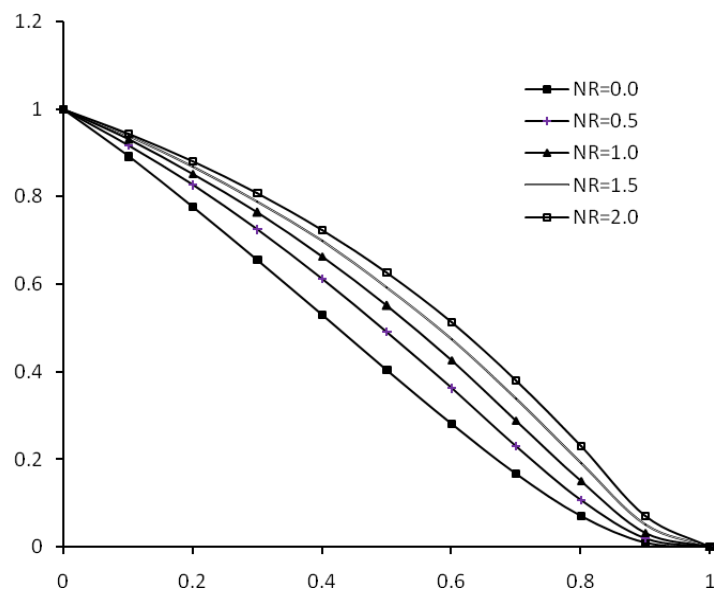
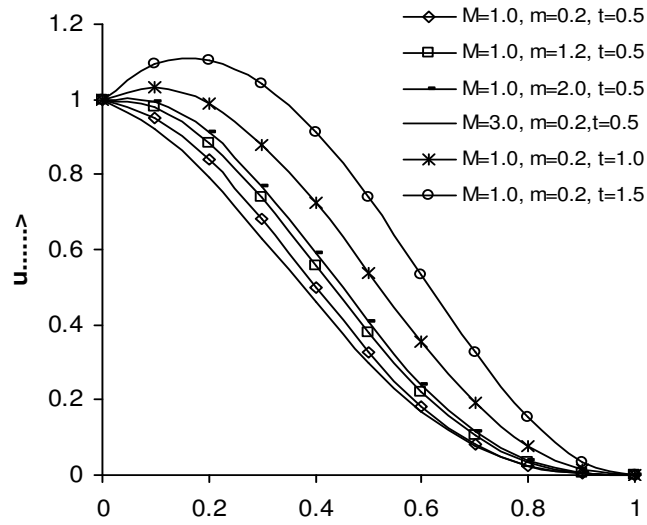


Fig 6: Effect of radiation (NR) on temperature field (θ)
 (Gr=5.0, Gm=5.0, m=1.0, M=1.0, Du=1.0, So=1.0, Pr=0.71, Ec=0.5, S=0.5, Ch=0.5, Sc=0.22, A=0.3 and \mathcal{E} =0.01)

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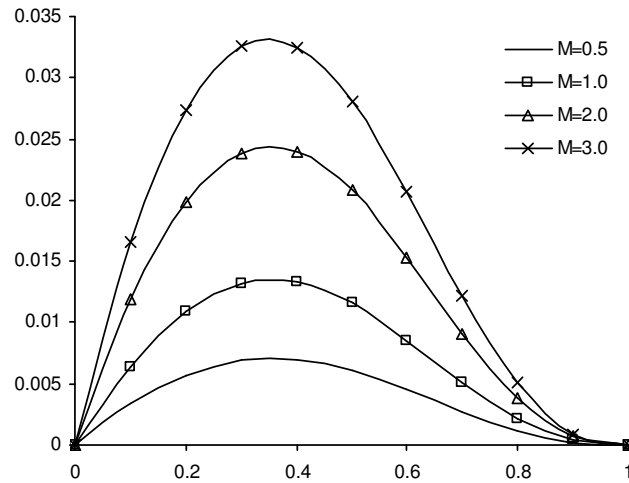


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Fig7: Effects of Magnetic field (M) and Hall current m on velocity field u
(Gr=5.0, Gm=5.0, NR=0.5, Ec=0.2, S=0.5, Pr=0.71, Sc=0.22, Kr=0.5, A=0.3 and \mathcal{E} =0.01)



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Fig8: Effects of Magnetic field (M) on velocity component W
(Gr=5.0, Gm=5.0, NR=0.5, Ec=0.2, S=0.5, Pr=0.71, Sc=0.22, Kr=0.5, A=0.3, \mathcal{E} =0.01 and t=1.0)

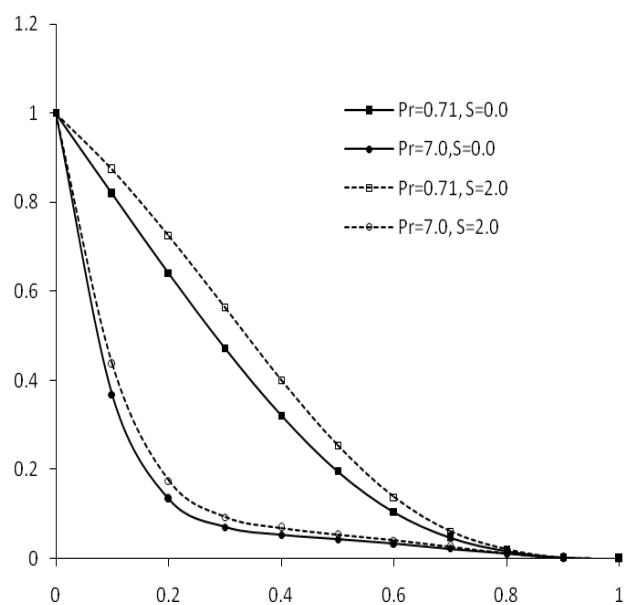


Fig 9: Effect of Prandtl number (Pr) on temperature field (Θ) in the presence of heat source
(Gr=5.0, Gm=5.0, m=1.0, M=1.0, Du=1.0, So=1.0, Ec=0.5, NR=0.5, Ch=0.5, Sc=0.22, A=0.3 and \mathcal{E} =0.01)

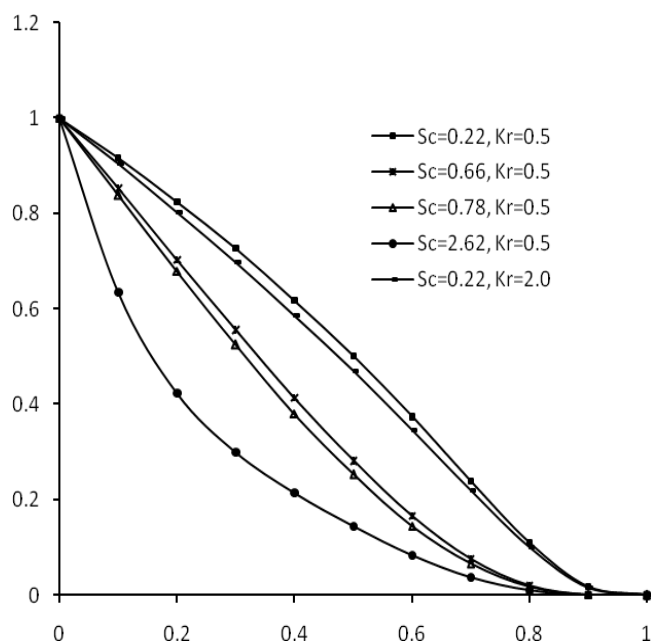


Fig 10: Effect of Schmidt number and chemical reaction on Concentration field
(NR=0.5, Pr=0.71, \square =0.01, n=0.1, A=0.3 and t=1.0)

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