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- 7 8 Abstract
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Original Research Article

COMBINED EFFECTS OF HALL CURRENT AND MAGNETIC FIELD ON UNSTEADY FLOW PAST <mark>A</mark> SEMI-INFINITE VERTICAL PLATE WITH THERMAL RADIATION AND HEAT SOURCE

10 In the present study combined effects of Hall current and magnetic field on unsteady 11 laminar boundary layer flow of a chemically reacting incompressible viscous fluid 12 along a semi-infinite vertical plate with thermal radiation and heat source is analyzed 13 numerically. A magnetic field of uniform strength is applied normal to the flow. 14 Viscous dissipation and thermal diffusion effects are included. In order to establish a 15 finite boundary condition $(\eta \rightarrow 1)$ instead of an infinite plate condition, the governing 16 equations in non- dimensional form are transformed to new system of co-ordinates. 17 Obtaining exact solution for this new system of differential equations is very difficult 18 due to its coupled non-linearity, so they are transformed to system of linear equations 19 using implicit finite difference formulae and these are solved using 'Gaussian 20 elimination' method and for this simulation is carried out by coding in C-Program. 21 Graphical results for velocity, temperature and concentration fields are presented and 22 discussed. The results obtained for skin-friction coefficient, Nusselt and Sherwood 23 numbers are discussed and compared with previously published work in the absence 24 of Hall current parameter. These comparisons have shown a good agreement between 25 the results. A research finding of this study, achieved that the velocity and temperature 26 profiles are severely affected by the Hall effect and magnetic field and also a 27 considerable enhancement in temperature, main and secondary flow velocities of the 28 fluid is observed for increasing values of radiation parameter.

29

30 Key words:

Hall current, magnetic field, radiative heat flux, chemical reaction, Implicit finitedifference method,

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36 **1. Introduction**

35

37 Considerable attention has been given to the unsteady free-convection flow of viscous 38 incompressible, electrically conducting fluid in the presence of applied magnetic field 39 in connection with the theory of fluid motion in the liquid core of the earth, 40 meteorological and oceanographic applications. Due to the gyration and drift of 41 charged particles, the conductivity parallel to the electric field is reduced and the 42 current is induced in the direction normal to both electric and magnetic fields. This 43 phenomenon is known as the 'Hall effect'. This effect on the fluid flow with variable 44 concentration has a lot of applications in MHD power generators, general 45 astrophysical and meteorological studies and it can be taken into account within the 46 range of magneto hydro dynamical approximations. Hiroshi Sato [1] has studied the 47 effect of Hall current on the steady hydro magnetic flow between two parallel plates. 48 Masakazu Katagiri [2] studied the steady incompressible boundary layer flow past a 49 semi infinite flat plate in a transverse magnetic field at small magnetic Reynolds 50 number considering with the effect of Hall current. On the other hand Hossain [3] 51 studied the unsteady flow of incompressible fluid along an infinite vertical porous flat plate subjected to suction/injection velocity proportional to (time)^{-1/2}. Hossain and 52 53 Rashid [4] investigated the effect of Hall current on the unsteady free convection flow 54 of a viscous incompressible fluid with mass transfer along a vertical porous plate 55 subjected to a time dependent transpiration velocity when the constant magnetic field is applied normal to the flow. Sri Gopal Agarwal [5] discussed the effect of hall 56 57 current on the unsteady hydro magnetic flow of viscous stratified fluid through a 58 porous medium in the free convection currents. Ajay Kumar Singh [6] analyzed the 59 steady MHD free convection and mass transfer flow with Hall current, viscous 60 dissipation and joule heating, taking in to account the thermal diffusion effect. In all 61 these studies, the effect of Hall current with radiation on the flow field has not been 62 discussed.

64 Several authors have dealt with heat flow and mass transfer over a vertical porous 65 plate with variable suction, heat absorption/ generation, radiation and chemical 66 reaction. Actually many process in engineering areas occur at high temperature and 67 knowledge of radiation heat transfer becomes very important for the design of the 68 pertinent equipment. Nuclear power plants, gas turbines and the various propulsion devices for air craft, missiles, satellites and space vehicles are examples of such 69 70 engineering areas. In such cases one has to take into account the effects of radiation. 71 So, Perdikis and Raptis [7] illustrated the heat transfer of a micro polar fluid in the 72 presence of radiation. Takhar et al. [8] considered the effects of radiation on free-73 convection flow of a radiation gas past a semi infinite vertical plate in the presence of 74 magnetic field. Raptis and Massalas [9] studied the magneto-hydrodynamic flow past 75 a plate by the presence of radiation. Elbashbeshby and Bazid [10] have reported the 76 effect of radiation on forced convection flow of a micro polar fluid over a horizontal 77 plate. Chamka et al. [11] studied the effect of radiation on free convection flow past a 78 semi infinite vertical plate with mass transfer. Ganeshan and Loganathan [12] 79 analyzed the radiation and mass transfer effects on flow of an incompressible viscous 80 fluid past a moving cylinder. Kim et al. [13] analyzed the effect of radiation on 81 transient mixed convection flow of a micropolar fluid past a moving semi infinite 82 vertical porous plate. Makinde [14] examined the transient free convection interaction 83 with thermal radiation of an absorbing-emitting fluid. Perdikis and Rapti [15] 84 discussed unsteady magnetic hydrodynamic flow in the presence of radiation.

85

86 Ramachandra Prasad et al. [16] considered the effects radiation and mass transfer on 87 two dimensional flow past an infinite vertical plate. Chaudhary and Preethi Jain [17] 88 presented an analysis to study the effects of radiation on the hydromagnetic free 89 convection flow of an electrically conducting micropolar fluid past a vertical porous 90 plate through a porous medium in slip-flow regime. The effect of thermal radiation, 91 time-dependent suction and chemical reaction on the two-dimensional flow of an 92 incompressible Boussinesq fluid, applying a perturbation technique has been studied 93 by Prakash and Ogulu [18]. Later, for this same study a numerical investigation is 94 carried out by Rajireddy and Srihari [19]. Ibrahim et al. [20] analyzed the effects of the

95 chemical reaction and radiation absorption on transient hydro-magnetic free-96 convention flow past a semi infinite vertical permeable moving plate with wall 97 transpiration and heat source. SudheerBabu and Satyanarayana [21] discussed the 98 effects of the chemical reaction and radiation absorption in the presence of magnetic 99 field on free convection flow through porous medium with variable suction. Dulalpal 100 and Babulal Talukdar [22] has made the perturbation analysis to study the effects 101 thermal radiation and chemical reaction on magneto-hydrodynamic unsteady heat and 102 mass transfer in a boundary layer flow past a vertical permeable plate in the slip flow regime. Satyanarayana et al. [23] studied the steady magneto-hydrodynamic free 103 104 convection viscous incompressible fluid flow past a semi infinite vertical porous plate 105 with mass transfer and hall current. Anand Rao et al. [24] analyzed the effects of viccous dissipation and Soret on an unsteady two-dimensional laminar mixed 106 107 convective boundary layer flow of a chemically reacting viscous incompressible fluid, 108 along a semi-infinite vertical permeable moving plate. Satyanarayana et al. [25] 109 analyzed the effects of Hall current and radiation absorption on magneto-110 hydrodynamic free convection flow of a micropolar fluid in a rotating frame of 111 reference. Harish Babu and Satya Narayana [26] discussed the variation of 112 permeability and radiation on the heat and mass transfer flow micropolar fluid along a 113 vertical moving porous plate by considering the effect of transverse magnetic field in 114 to account. In addition to this, Satyanarayana et al. [27] studied the effects of chemical 115 reaction and radiation absorption on magneto-hydrodynamic free-convection flow of a 116 micropolar fluid in a rotating system with heat source. Recently, Srihari and Kesava 117 **Reddy** [28] have made the numerical investigation to study the effects of soret and 118 magnetic field on unsteady laminar boundary layer flow of a radiating and chemically 119 reacting incompressible viscous fluid along a semi-infinite vertical plate. More 120 recently, Srihari and Srinivas Reddy [29] studied the effects of radiation and soret 121 number variation in the presence of heat source/sink on unsteady laminar boundary 122 layer flow of chemically reacting incompressible viscous fluid along a semi-infinite 123 vertical plate with viscous dissipation.

125 In most of the earlier studies analytical or perturbation methods were applied to 126 obtain the solution of the problem and there seems to be no significant consideration 127 of the combined effects of Hall current and magnetic field with thermal radiation. 128 Moreover, when the radiative heat transfer takes place, the fluid involved can be 129 electrically conducting in the sense that it is ionized owing to the high operating 130 temperature. Accordingly, it is of interest to examine the effect of magnetic field on 131 the flow and when the strength of applied magetic field is strong, one cannot neglect 132 the effect of Hall current. So in the present study the combined effects of magnetic field and Hall current on unsteady laminar flow of a chemically reacting 133 134 incompressible viscous fluid along a semi-infinite vertical plate with thermal radiation 135 is investigated. A magnetic field of uniform strength is applied normal to the fluid flow.In order to obtain the approximate solution and to describe the physics of the 136 137 problem, the present non-linear boundary value problem is solved numerically using 138 implicit finite difference formulae known as Crank-Nicholson method. The obtained 139 results are discussed in detail and compared with the results of Skin-friction, Nusselt 140 and Sher-wood numbers, presented by Srihari and Srinivas Reddy [29] in the absence 141 of Hall current parameter.

142

143 **2. Formulation of the problem**

144 An unsteady laminar, boundary layer flow of a viscous, incompressible, electrically 145 conducting dissipative and chemically reacting fluid along a semi-infinite vertical plate, with thermal radiation, heat source is considered. The x'-axis taken along the 146 plate in the vertically upward direction and y'-axis normal to it. A magnetic field of 147 uniform strength applied along y'-axis. Further, due to the semi-infinite plane surface 148 assumption, the flow variables are functions of normal distance y' and t' only. A time 149 150 dependent suction velocity is assumed normal to the plate. A magnetic field of 151 uniform strength is assumed to be applied transversely to the porous plate. The 152 magnetic Reynolds number of the flow is taken to be small enough so that the induced 153 magnetic field can be neglected. The equation of conservation of electric charge $\nabla . \vec{J} = 0$, gives $j_y = \text{constant}$, where $\vec{J} = (j_x, j_y, j_z)$. We further assume that the 154

plate is non-conducting. This implies $j_y = 0$ at the plate and hence zero everywhere. When the strength of magnetic field is very large the generalized Ohm's law, in the absence of electric field takes the following form:

159
$$\vec{J} + \frac{\omega_e \,\tau_e}{B_0} (\vec{J} \times \vec{B}) = \sigma \left(\vec{V} \times \vec{B} + \frac{1}{en_e} \,\nabla P_e \right) \tag{1}$$

Where V is the velocity vector, σ is the electric conductivity, ω_e is the electron frequency, τ_e is the electron collision time, e is the electron charge, n_e is the number density of the electron and P_e is the electron pressure. Under the assumption that the electron pressure (for weakly ionized gas), the thermo-electric pressure and ion-slip are negligible, equation (2.1) becomes:

166
$$J_x = \frac{\sigma B_0}{1+m^2} (mu - w) \text{ and } j_z = \frac{\sigma B_0}{1+m^2} (u+mw)$$
 (2)

where u is the x-component of V, w is the z component of V and $m(=w_e \tau_e)$ is the Hall parameter.

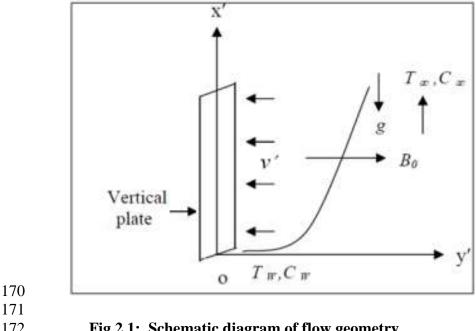


Fig 2.1: Schematic diagram of flow geometry

Within the above framework, the equations which govern the flow under the usualBoussinesq approximation are as follows:

176

178
$$\frac{\partial v'}{\partial y'} = 0$$
 (3)

179

- 180 Momentum equations
- 181

182
$$\frac{\partial u'}{\partial t'} + v' \frac{\partial u'}{\partial y'} = v \frac{\partial^2 u'}{\partial y'^2} + g\beta(T - T_{\infty}) + g\beta^* (C - C_{\infty}) - \frac{\sigma B_0^2}{\rho(1 + m^2)} (u' + mw')$$
(4)

183

184
$$\frac{\partial w'}{\partial t'} + v' \frac{\partial w'}{\partial y'} = v \frac{\partial^2 w'}{\partial y'^2} - \frac{\sigma B_0^2}{\rho(1+m^2)} (w' - mu')$$
(5)

185

186 • Energy

187
$$\frac{\partial T}{\partial t'} + v' \frac{\partial T}{\partial y'} = \frac{k}{\rho C_p} \frac{\partial^2 T}{\partial {y'}^2} - \frac{1}{\rho c_p} \frac{\partial q_r}{\partial y'} + \frac{\mu}{\rho c_p} \left(\frac{\partial u'}{\partial y'}\right)^2 + \frac{Q(T - T_{\infty})}{\rho c_p}$$
(6)

188

189 • Mass transfer

190
$$\frac{\partial C}{\partial t'} + v' \frac{\partial C}{\partial y'} = D \frac{\partial^2 C}{\partial y'^2} + \frac{D_m k_T}{T_m} \frac{\partial^2 T}{\partial y'^2} - k_r^2 C$$
(7)

191

192 The radiative flux q_r by using the Rosseland approximation [30], is given by 193

194
$$q_r = -\frac{4\sigma^*}{3a_R} \frac{\partial T^4}{\partial y'}$$
(8)

195 The boundary conditions suggested by the physics of the problem are

$$u' = U_0, w' = 0, T = T_w + \varepsilon (T_w - T_\infty) e^{n't'}, C = C_w + \varepsilon (C_w - C_\infty) e^{n't'} \quad at \quad y' = 0$$

$$u' \to 0, w' = 0, T \to T_\infty, C \to C_\infty \qquad as \quad y' \to \infty$$
(9)

197 It has been assumed that the temperature differences within the flow are sufficiently 198 small and T^4 may be expressed as a linear function of the temperature *T* using Taylor 199 series as follows

200 Let the Taylor series about
$$T_{\infty}$$
, be $T^4 = T_{\infty}^4 + 4(T - T_{\infty})T_{\infty}^3 + 12\frac{(T - T_{\infty})^2}{2!}T_{\infty}^2 + \dots$

²⁰¹ Neglecting the higher order terms in the above series, we have

202
$$T^4 \approx 4T_{\infty}^3 T - 3T_{\infty}^4$$
 (10)

203 Using (10) in (8) and then (8) in (6), it implies

$$205 \qquad \frac{\partial T}{\partial t'} + v' \frac{\partial T}{\partial y'} = \frac{k}{\rho c_p} \frac{\partial^2 T}{\partial y'^2} - \frac{16\sigma^* T_{\infty}^3}{3\rho c_p k^*} \frac{\partial^2 T}{\partial y'^2} + \frac{\mu}{\rho c_p} \left(\frac{\partial u'}{\partial y'}\right)^2 + \frac{Q(T - T_{\infty})}{\rho c_p}$$
(11)

206

207 Integration of continuity eqn (1) for variable suction velocity normal to the plate gives
208
$$v' = -U_0 \left(1 + \varepsilon A e^{n't'}\right)$$
 (12)

where *A* is the suction parameter and εA is less than unity. Here U_0 is mean suction velocity, which is a non-zero positive constant and the minus sign indicates that the suction is towards the plate.

In order to obtain the non-dimensional partial differential equations with boundaryconditions, introducing the following non-dimensional quantities,

214

215
$$u = \frac{u'}{U_0}, \quad w = \frac{w'}{U_0}, \quad y = \frac{y'U_0}{v}, \quad t = \frac{U_0^2 t'}{v}, \quad \theta = \frac{T - T_\infty}{T_w - T_\infty},$$

216
$$\phi = \frac{C - C_{\infty}}{C_w - C_{\infty}}, \text{ Pr} = \frac{\mu C_p}{k}, \text{ Sc} = \frac{\nu}{D}, M = \frac{\sigma B_0^2 \nu}{\rho U_0^2}, \text{ So} = \frac{D_m k_T (T_w - T_{\infty})}{\nu T_m (C_w - C_{\infty})}$$

217
$$Gr = \frac{g\beta v(T_w - T_w)}{U_0^3}, \quad Gm = \frac{g\beta^* v(C_w - C_w)}{U_0^3}, \quad S = \frac{Qv}{\rho C_p U_0^2}$$
(13)

218

219
$$Kr = \frac{k_r^2 \upsilon}{U_0^2}, \ NR = \frac{16\sigma^* T_{\infty}^3}{3ka_R}, \ Ec = \frac{U_0^2}{C_p (T_w - T_{\infty})} \quad n = \frac{\upsilon n'}{U_0^2}, \text{ in to equations (4), (5),}$$

220 (7) and (11), we get

221
$$\frac{\partial u}{\partial t} - \left(1 + \varepsilon A e^{nt}\right) \frac{\partial u}{\partial y} = \frac{\partial^2 u}{\partial y^2} - \frac{M}{1 + m^2} \left(u + mw\right) + Gr\theta + Gm\phi$$
(14)

222
$$\frac{\partial w}{\partial t} - \left(1 + \varepsilon A e^{nt}\right) \frac{\partial w}{\partial y} = \frac{\partial^2 w}{\partial y^2} - \frac{M}{1 + m^2} (w - mu)$$
(15)

223
$$\frac{\partial\theta}{\partial t} - \left(1 + \varepsilon A e^{nt}\right) \frac{\partial\theta}{\partial y} = \left(\frac{1 + NR}{Pr}\right) \frac{\partial^2\theta}{\partial y^2} + Ec \left(\frac{\partial u}{\partial y}\right)^2 + S\theta$$
(16)

224
$$\frac{\partial \phi}{\partial t} - \left(1 + \varepsilon A e^{nt}\right) \frac{\partial \phi}{\partial y} = \frac{1}{Sc} \frac{\partial^2 \phi}{\partial y^2} + So \frac{\partial^2 \theta}{\partial y^2} - Kr\phi$$
(17)

- 225
- 226 with the boundary conditions

227
$$u = 1, w = 0, \theta = 1 + \varepsilon e^{nt}, \phi = 1 + \varepsilon e^{nt}$$
 at $y = 0$

228
$$u \to 0, w = 0, \ \theta \to 0, \ \phi \to 0$$
 as $y \to \infty$ (18)
229

In order to establish a finite plate condition, $\eta \rightarrow 1$ in equation (18) instead of an infinite boundary condition, $y \rightarrow \infty$, employing the transformation $\eta = 1 - e^{-y}$ on equations (14)-(18), we get

234
$$\frac{\partial u}{\partial t} - \left(1 + \varepsilon A e^{nt}\right) (1 - \eta) \frac{\partial u}{\partial \eta} = (1 - \eta)^2 \frac{\partial^2 u}{\partial \eta^2} - (1 - \eta) \frac{\partial u}{\partial \eta} - \frac{M}{1 + m^2} (u + mw) + Gr\theta + Gm\phi$$
235 (19)

236
$$\frac{\partial w}{\partial t} - \left(1 + \varepsilon A e^{nt}\right) (1 - \eta) \frac{\partial w}{\partial \eta} = (1 - \eta)^2 \frac{\partial^2 w}{\partial \eta^2} - (1 - \eta) \frac{\partial w}{\partial \eta} - \frac{M}{1 + m^2} (w - mu)$$
(20)

237
$$\frac{\partial\theta}{\partial t} - \left(1 + \varepsilon A e^{nt}\right)\left(1 - \eta\right)\frac{\partial\theta}{\partial\eta} = \left(\frac{1 + NR}{Pr}\right)\left(\left(1 - \eta\right)^2\frac{\partial^2\theta}{\partial\eta^2} - (1 - \eta)\frac{\partial\theta}{\partial\eta}\right) + Ec\left((1 - \eta)\frac{\partial u}{\partial\eta}\right)^2 + S\theta$$
238 (21)

239
$$\frac{\partial \phi}{\partial t} - \left(1 + \varepsilon A e^{nt}\right) (1 - \eta) \frac{\partial \phi}{\partial \eta} = \frac{1}{Sc} \left((1 - \eta)^2 \frac{\partial^2 \phi}{\partial \eta^2} - (1 - \eta) \frac{\partial \phi}{\partial \eta} \right) + So \left((1 - \eta)^2 \frac{\partial^2 \theta}{\partial \eta^2} - (1 - \eta) \frac{\partial \theta}{\partial \eta} \right) - Kr\phi$$
(22)

240 with boundary conditions

241

u = 1: w = 0, $\theta = 1 + \varepsilon e^{nt}$, $\phi = 1 + \varepsilon e^{nt}$ at $\eta = 0$ 242 (23) $u \to 0: w = 0, \ \theta \to 0, \qquad \theta \to 1 + \varepsilon e^{nt} \quad as \ \eta \to 1$

243

244 3. Method of solution

Equations (19)-(22) are non-linear coupled, differential equations, for which obtaining 245 246 exact solution is very difficult, so they are transformed to system of linear equations 247 using implicit finite difference formulae, as follows

248
$$-P_3 r u_{i-1}^{j+1} + (1+2P_3 r) u_i^{j+1} - P_3 r u_{i+1}^{j+1} = E_i^j$$
(24)

249
$$-P_3 r w_{i-1}^{j+1} + (1+2P_3 r) w_i^{j+1} - P_3 r w_{i+1}^{j+1} = D_i^j$$
(25)

250
$$-P_{3}P_{4} r \theta_{i-1}^{j+1} + (1 + 2P_{3}P_{4} r)\theta_{i}^{j+1} - P_{3}P_{4} r \theta_{i+1}^{j+1} = F_{i}^{j}$$
251 (26)

252
$$-\frac{P_3 r}{Sc} \phi_{i-1}^{j+1} + \left(1 + \frac{2P_3 r}{Sc}\right) \phi_i^{j+1} - \frac{P_3 r}{Sc} \phi_{i+1}^{j+1} = H_i^j$$
(27)

253

254 with boundary conditions in finite difference form 255

256
$$\begin{array}{c} u\left(0,j\right) = 1, \quad \theta(0,j) = 1 + \varepsilon \exp(n,j,k_1), \quad \phi = 1 + \varepsilon \exp(n,j,k_1), \quad \forall j \\ u(10,j) \to 0, \quad \theta(10,j) \to 0, \quad \phi(10,j) \to 1 \quad \forall j \end{array}$$
 (28)

257 where

$$E_{i}^{j} = P_{3}r u_{i-1}^{j} - \left(1 - P_{1}P_{2}rh - 2P_{3}r + P_{2}rh - \frac{Mm}{1 + m^{2}}k_{1}\right)u_{i}^{j} + \left(P_{1}P_{2}rh + P_{3}r - P_{2}rh\right)u_{i+1}^{j}$$
258
$$+ Gr k_{1}\theta_{i}^{j} + Gm k_{1}\phi_{i}^{j} - \frac{Mm}{1 + m^{2}}k_{1} w_{i}^{j}$$

260
$$D_{i}^{j} = P_{3}r w_{i-1}^{j} - \left(1 - P_{1}P_{2}rh - 2P_{3}r + P_{2}rh - \frac{Mm}{1 + m^{2}}k_{1}\right)w_{i}^{j} + \left(P_{1}P_{2}rh + P_{3}r - P_{2}rh\right)w_{i+1}^{j} + \frac{Mm}{1 + m^{2}}k_{1}u_{i}^{j}$$

261
$$F_{i}^{j} = P_{3}P_{4}r\theta_{i-1}^{j} + (1 - P_{1}P_{2}rh - 2P_{3}P_{4}r + P_{2}P_{4}rh)\theta_{i}^{j} + (P_{1}P_{2}rh + P_{3}P_{4}r - P_{2}P_{4}rh)\theta_{i+1}^{j}$$
262

264
$$H_{i}^{j} = \frac{P_{3}r}{Sc} \phi_{i-1}^{j} + \left(1 + P_{1}P_{2}rh - \frac{2P_{3}r}{Sc} + \frac{P_{2}rh}{Sc} - k_{r}^{2}k_{1}\right)\phi_{i}^{j} + \left(\frac{P_{3}r}{Sc} - P_{1}P_{2}rh - \frac{P_{2}rh}{Sc}\right)\phi_{i+1}^{j} + \left(2P_{3}rS_{0} - S_{0}P_{1}rh\right)\theta_{i+1}^{j} + \left(S_{0}P_{1}rh - 4P_{3}rS_{0}\right)\theta_{i}^{j} + 2P_{3}rS_{0}\theta_{i-1}^{j}$$

265

266
$$P_1 = 1 + \in Ae^{nt}, P_2 = 1 - ih, P_3 = \frac{(1 - ih)^2}{2}, P_4 = \frac{1 + NR}{Pr},$$

where $r = k_1 / h^2$ and *h*, k_1 are mesh sizes along η and time direction respectively. Index *i* refers to space and *j* for time.

270

271 To obtain the difference equations, the region of the flow is divided into a grid or 272 mesh of lines parallel to η and t axes. Solutions of difference equations are obtained 273 at the intersection of these mesh lines called nodes. The finite-difference equations at 274 every internal nodal point on a particular *n*-level constitute a tri-diagonal system of 275 equations. These equations are solved by Gaussian elimination method and for this a 276 numerical code is executed using C-Program to obtain the approximate solution of the 277 system. In order to prove the convergence of present numerical scheme, the 278 computation is carried out by slightly changed values of h, and k_1 , and the iterations on until a tolerance 10^{-8} is attained. No significant change was observed in the values 279 280 of u, w, θ and ϕ . Thus, it is concluded that the finite difference scheme is convergent 281 and stable.

282

283 Skin-friction

284 The Skin friction coefficient τ is given by

285

286
$$\tau = \frac{\partial u}{\partial y}\Big|_{y=0} = (1-\eta)\frac{\partial u}{\partial \eta}\Big|_{\eta=0},$$
287 (29)

288

289 Nusselt number

290 The rate of heat transfer in terms of Nusselt number is given by

292
$$Nu = \frac{\partial \theta}{\partial y}\Big|_{y=0} = (1-\eta)\frac{\partial \theta}{\partial \eta}\Big|_{y=0}$$
(30)

294 Sherwood number295

- 296 The coefficient of Mass transfer which is generally known as Sherwood number, Sh, is
- 297 given by

298
$$Sh = \frac{\partial \phi}{\partial y}\Big|_{y=0} = (1-\eta)\frac{\partial \phi}{\partial \eta}\Big|_{\eta=0}$$
 (31)

299Nomenclature

ρ	Density
C_p	Specific heat at constant pressure
V	Kinematic viscosity
k	Thermal conductivity
U	Mean velocity
Sc	Schmidt number
Т	Temperature
k_r^2	Chemical reaction rate constant
E	Small reference parameter << 1
Pr	Prandtl number
Gr	Free convection parameter due to temperature
Gm	Free convection parameter due to concentration
т	Hall current
Α	Suction parameter
n	A constant exponential index
D	Molar diffusivity
NR	Thermal radiation parameter
β	Coefficient of volumetric thermal expansion of the fluid
β^*	Volumetric coefficient of expansion with concentration
М	Magnetic parameter

σ	Electrical conductivity
$arma_{e}$	Eectron frequency
$ au_e$	Eectron collision time
е	Electron pressure
n _e	Number density of the electron
P _e	Electron pressure
So	Soret number
Ec	Viscous dissipation

Table 1 - Effects of Gr, Gm, Pr, Sc, Kr, NR $_{,}$ So and M on Skin-Friction coefficient 302 303

Gr	Gm	Pr	Sc	Kr	NR	So	М	T S=2.0,Ec=0.5 Previous [29] (m=0.0)	T S=2.0,Ec=0.5 Present (m=1.0)
5.0	5.0	0.71	0.24	0.5	0.5	0.0	0.0	1.4032	1.4032
5.0	5.0	0.71	0.24	0.5	0.5	0.0	2.0	0.7413	0.98796
5.0	5.0	0.71	0.24	0.5	0.5	2.0	2.0	0.9721	1.17426
5.0	5.0	0.71	0.24	0.5	1.0	2.0	2.0	1.0523	1.24643
5.0	5.0	0.71	0.6	0.5	0.5	2.0	2.0	0.8423	1.01633
5.0	5.0	7.0	0.24	0.5	0.5	2.0	2.0	0.3838	0.68666

5.0	<u>10.0</u>	0.71	0.24	0.5	0.5	2.0	2.0	2.7352	2.97588
10.0	5.0	0.71	0.24	0.5	0.5	2.0	2.0	2.3597	2.58178

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· 2	1 1	-	
- 1	.,	1	

Table 2 - Effects of NR and Pr on Nusselt - number

306			Nu	Nu
307	NR	Pr	S=2.0,Ec=0.5	S=2.0, Ec=0.5
308			Previous [29] (m=0.0)	Present (m=1.0)
500	0.0	0.71	-1.0807	-0.93922
309				
	0.5	0.71	-0.8230	-0.72087
310				
	0.5	7.0	-3.6770	-3.12927
311	0.7	11.4	4.550.4	4.00(51
	0.5	11.4	-4.7594	-4.03651
312				

313

314

Table 3 - Effects of Sc, Kr and So on Sherwood number

Sh

-0.43987

-0.55924

Sh

-0.59393

-0.37652

-0.44012

-0.56102

315

316			G .	S=2.0,Ec=0.5	S=2.0, Ec=0.5
510	Sc	Kr	So	Previous [29]	Present
317				(m=0.0)	(m=1.0)

2.0

2.0

 317
 (m=0.0)

 0.24
 0.5
 0.0
 -0.59393

 318
 0.24
 0.5
 2.0
 -0.37159

 319
 0.24
 0.5
 2.0
 -0.37159

1.0

0.5

0.24

0.6

320

321

322

324 **Results and discussion**

In order to obtain the approximate solution and to describe the physics of the problem, in the present work, numerical solution is obtained to study the influence of various flow parameters encountered in the momentum, energy and mass transfer equations. To be realistic, the values of Prandtl number (Pr) are chosen to be Pr = 0.71 and Pr =7.0, which represent air and water at temperature 20 °C and one atmosphere pressure,

- 330 respectively.
- 331

332 Figures (1) and (2) show the effect of Hall current (m) on velocity field's u and w 333 respectively, in the presence of heat source. It is observed that the effect of increasing 334 values of m results in increasing both the velocity profiles u and w. This due to the fact that an increase in hall current produces a deflection on moving fluid so that the 335 336 level of cross flow velocity is maximum and therefore the fluid is dragged with more 337 velocity. Furthermore, it is noted that both the velocities u and w increase in the 338 presence of heat source as the internal heat generation is to increase the rate of heat 339 transport to the fluid. From figure (3), it is interesting to note that there is a 340 considerable enhancement in the secondary flow velocity of the fluid is observed for 341 slightly increasing values of Hall parameter.

342

343 From figures (4), (5) and (6), it is seen that for increasing values of NR, there is rise in 344 the temperature, main and cross flow velocities. This due to the fact that an increase in the value of radiation parameter $NR = 16\sigma^* T_{\infty}^3 / 3k a_R$, forgiven k and T_{∞} leads to 345 decrease in the Roseland radiation absorbtivity (a_R) . According to the equations (6) 346 and (8), it is concluded that, the divergence of the radiation heat flux $(\partial q_r / \partial y^*)$ 347 increases as a_R decreases and it implies that the rate of radiative heat, transferred to 348 349 the fluid increases and consequently the fluid temperature and therefore main and 350 secondary flow velocities of their particles also increase. Furthermore, it is interested 351 note that velocity u increases in the presence of radiation.

353 Figures (7) and (8) show the effect magnetic parameter M on main and cross flow 354 velocity profiles respectively. It is observed from figure (7) that an increase in M leads 355 to decrease in the velocity. This due to the fact that the introduction of transverse magnetic 356 field in an electrically conducting fluid has a tendency to give rise to a resistive-type force 357 called the Lorentz force, which acts against the fluid flow and hence results in retarding the 358 velocity profile. Furthermore, from figure (8) it is seen that for increasing values magnetic 359 parameter M, there is a considerable enhancement in the cross flow velocity w, as the 360 impact of deflecting force due to the applied magnetic field on the fluid is predominant. 361

The effect Prandtl number in the presence of heat source parameter on temperature distribution is shown in figure (9). It is evident from figure that the temperature increases in the presence of heat source parameter as the effect of internal heat generation is to increase the rate of heat transport to the fluid. Furthermore it is interesting to note that with increasing values of Prandtl number Pr, there is a decrease in the temperature profile. This due to the physical fact that an increase in Pr leads to decrease in the thermal boundary layer thickness.

369

Fig (10) shows the species concentration for different gases like Hydrogen (H2: Sc=0.22), Oxygen (O2: Sc=0.66), Ammonia (NH3 : Sc=0.78) and $S_c = 2.62$ for propyl benzene at 20°C and one atmospheric pressure and for different Kr. It is observed that the effect of increasing values of chemical reaction parameter and Schmidth number is to decrease concentration distribution in the flow region.

375 376

Results for Skin-friction coefficient, Nusselt and Sherwood numbers are presented in tables (1), (2) and (3) respectively, in the presence and absence of Hall effect. A comparative numerical study between present and previous results in tables reveals that Skin–friction, Nusselt number increase in the presence of Hall current parameter but Sherwood number decreases slightly in the presence of Hall effect. Further, it is noted that Skin-friction increases with increasing values of m, NR, Ec, So, Gr and Gm while it decreases for the increasing values of M, Pr. An increase in Ec, m, S leads to an increase in the Nusselt number. For increasing values of Sc and Ch decreases theSherwood number. But it increases with the increasing values So.

386

In order to access the validity of the present numerical scheme, the present results are compared with previous published data [29] for Skin-friction, rate of heat and mass transfer in the absence of Hall effect. The comparisons in all the cases are found to be in very good agreement and it gives an indication of high degree of coincidence with realistic physical phenomenon.

392

5. Conclusions:

394 Combined effects of Hall current and Magnetic field on unsteady laminar flow of a 395 radiating fluid along a semi-infinite vertical plate, with heat source, viscous dissipation 396 and thermal diffusion are analysed. From this study the following conclusions are 397 drawn.

- The velocity and temperature profiles are severely affected by the magnetic
 field and Hall effects.
- 400400401<l
- 402 3. Magnetic field reduces the main flow velocity profile but there is a
 403 considerable enhancement in the cross flow velocity is observed for increasing
 404 values same magnetic parameter M.
- 405
 4. Skin–friction, Nusselt increase in the presence of Hall effect. The temperature,
 406
 velocity, Skin–friction and Nusselt number increase in the presence heat source
- 407 5. There is a rise in the temperature, primary and secondary velocities of the fluid408 flow for increasing values of radiation parameter.
- 409
 6. The comparative study, between present and previously published results [29] for
 410
 410 Skin-friction, Nusselt and Sherwood numbers in the absence of Hall
 411 parameter, shows a good agreement. And therefore it is concluded that the
 412 proposed numerical technique, present in the paper is an efficient algorithm
 413 with assured convergence.

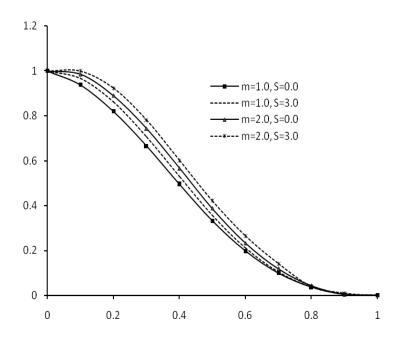
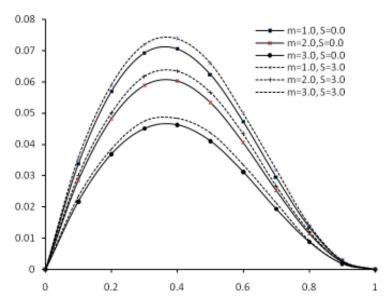


Fig1: Effect of Hall current (m) on velocity field u in the presence of heat source (Gr=5.0, Gm=5.0, M=1.0, Du=1.0, Pr=0.71, Ec=0.5, NR=0.5, Ch=0.5, So=1.0, Sc=0.22, A=0.3 and \mathcal{E} =0.01)

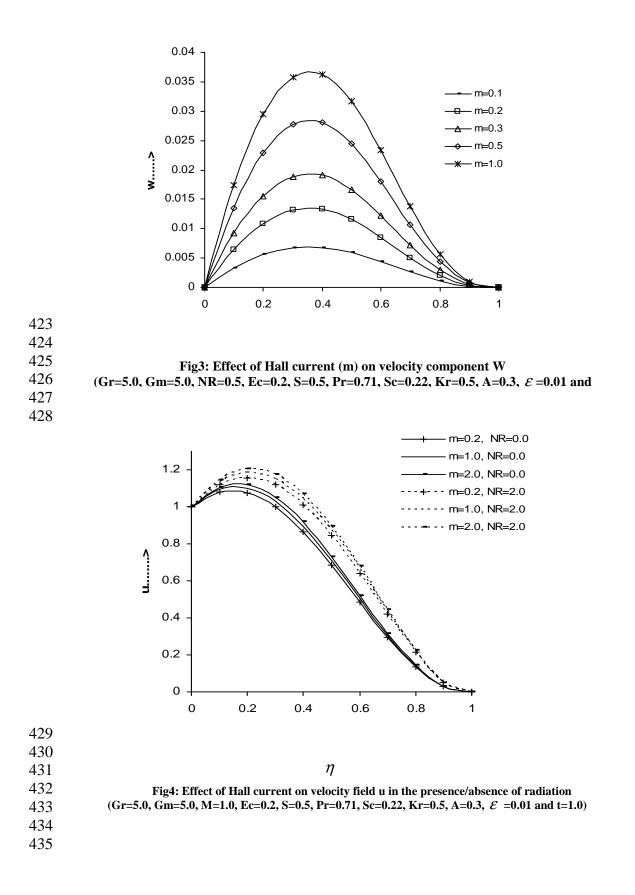


 418
 Fig 2: Effect of Hall current (m) on velocity field w in the presence of heat source

 419
 (Gr=5.0, Gm=5.0, M=1.0, So=1.0, Du=1.0, Pr=0.71, Ec=0.5, NR=0.5, Ch=0.5, Sc=0.22, A=0.3 and \mathcal{E} =0.01)

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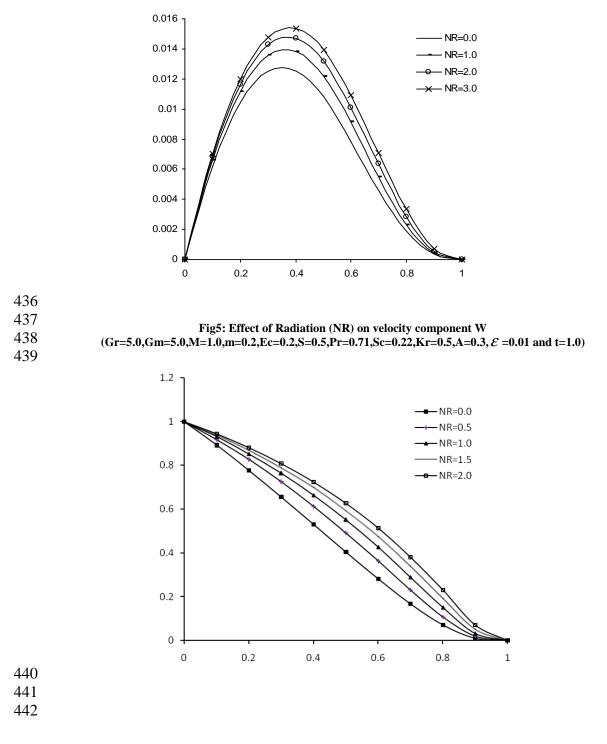
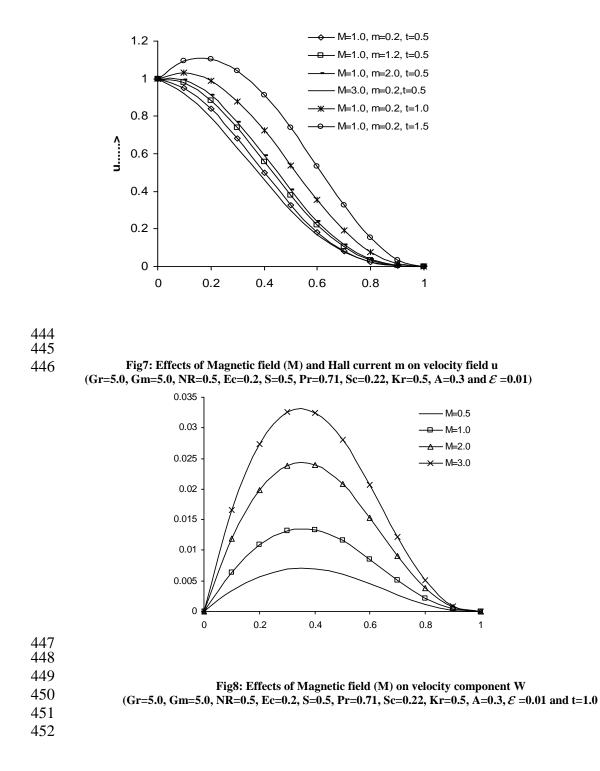
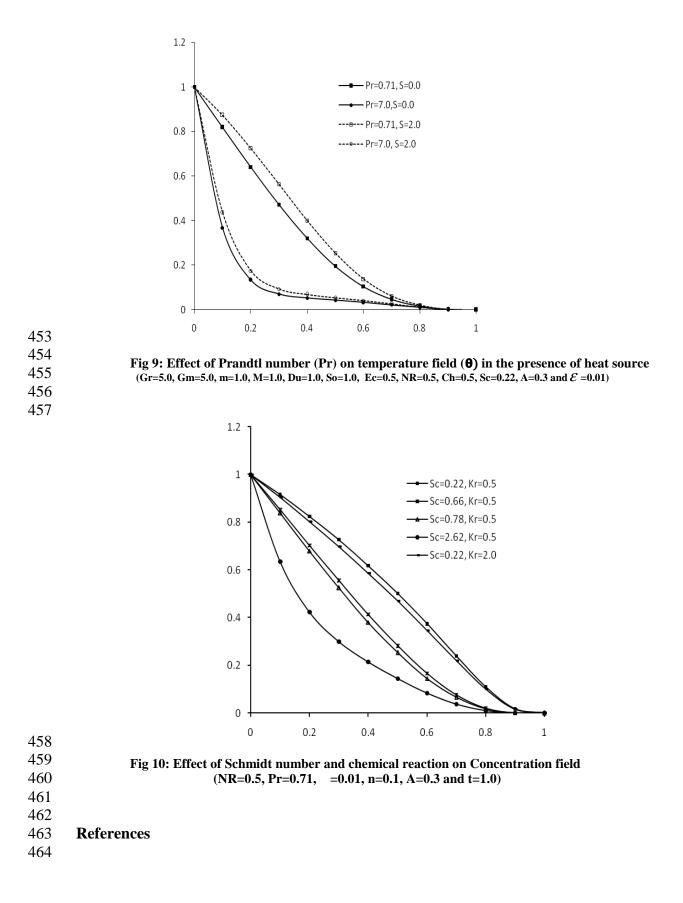


Fig 6: Effect of radiation (NR) on temperature field (θ) (Gr=5.0, Gm=5.0, m=1.0, M=1.0, Du=1.0, So=1.0, Pr=0.71, Ec=0.5, S=0.5, Ch=0.5, Sc=0.22, A=0.3 and \mathcal{E} =0.01)





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